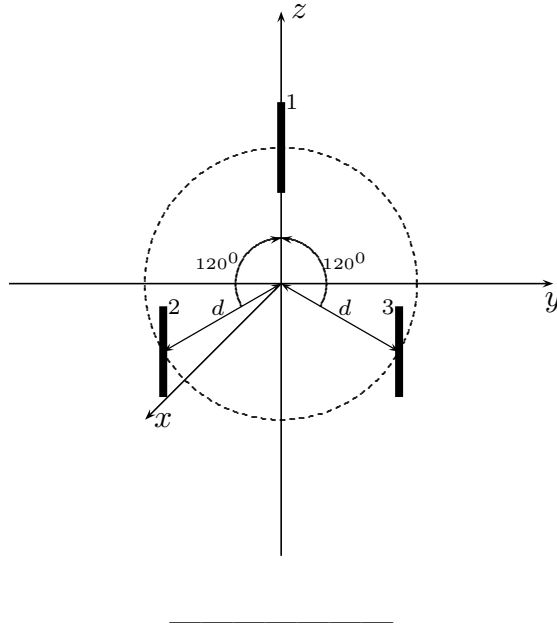


**Esercizi svolti di Campi elettromagnetici - Anno 2011**

**11-1) Esercizio n. 1 del 4/2/2011**

Sia dato un sistema di 3 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate nel piano  $yz$ , come in figura. Determinare l'espressione del vettore di Poynting irradiato.



(vedi es. n.1 del 22/9/2003)

Le densità di corrente sull'antenna 1, sull'antenna 2 e sull'antenna 3 sono rispettivamente:

$$\begin{cases} \vec{J}^{(1)} = \hat{z}A_1\delta(x)\delta(y)\cos k(z - z_1) & z_1 - l \leq z \leq z_1 + l \\ \vec{J}^{(2)} = \hat{z}A_2\delta(x)\delta(y - y_2)\cos k(z - z_2) & z_2 - l \leq z \leq z_2 + l \\ \vec{J}^{(3)} = \hat{z}A_3\delta(x)\delta(y - y_3)\cos k(z - z_3) & z_3 - l \leq z \leq z_3 + l \end{cases}$$

Posto  $A_1 = A_2 = A_3 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante è la somma delle tre:

$$\vec{J} = \hat{z}\delta(x)\delta(y)\cos k(z - z_1) + \hat{z}\delta(x)\delta(y - y_2)\cos k(z - z_2) + \hat{z}\delta(x)\delta(y - y_3)\cos k(z - z_3)$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  è:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}')d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \\ &= \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y') \cos k(z' - z_1) dx' dy' dz' + \\ &+ \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y' - y_2) \cos k(z' - z_2) dx' dy' dz' + \\ &+ \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y' - y_3) \cos k(z' - z_3) dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \hat{z} \int_{z_1-l}^{z_1+l} e^{-ikz' \cos \theta} \cos k(z' - z_1) dz' + \\ &+ \hat{z} e^{-iky_2 \sin \theta \sin \phi} \int_{z_2-l}^{z_2+l} e^{-ikz' \cos \theta} \cos k(z' - z_2) dz' + \\ &+ \hat{z} e^{-iky_3 \sin \theta \sin \phi} \int_{z_3-l}^{z_3+l} e^{-ikz' \cos \theta} \cos k(z' - z_3) dz' \end{aligned}$$

Valutiamo  $\int_{z_i-l}^{z_i+l} e^{-ikz' \cos \theta} \cos k(z' - z_i) dz'$ .

Poniamo  $z' - z_i = u \implies dz' = du$ . Per  $z' = z_i - l \implies u = -l$ . Per  $z' = z_i + l \implies u = +l$ . Si ha, quindi:

$$\begin{aligned} \int_{z_i-l}^{z_i+l} e^{-ikz' \cos \theta} \cos k(z' - z_i) dz' &= e^{-ikz_i \cos \theta} \int_{-l}^{+l} e^{-iku \cos \theta} \cos kudu = \\ &= e^{-ikz_i \cos \theta} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \end{aligned}$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \hat{z} e^{-ikz_1 \cos \theta} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} + \\ &+ \hat{z} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} + \\ &+ \hat{z} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \end{aligned}$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

Si ha:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{e}_r \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} \left\{ e^{-ikz_1 \cos \theta} + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + \right. \\ & \left. + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \right\} - \\ & - \hat{e}_\theta \sin \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} \left\{ e^{-ikz_1 \cos \theta} + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + \right. \\ & \left. + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \right\} \end{aligned}$$

Dalla figura risulta:

$$\begin{aligned} z_1 = +d, \quad y_2 = -d \cos(30^\circ) = -\frac{\sqrt{3}}{2}d, \quad z_2 = -d \sin(30^\circ) = -\frac{d}{2}, \\ y_3 = +d \cos(30^\circ) = +\frac{\sqrt{3}}{2}d, \quad z_3 = -d \sin(30^\circ) = -\frac{d}{2} \end{aligned}$$

Quindi:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{e}_r \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} \left\{ e^{-ikd \cos \theta} + e^{+ik\frac{\sqrt{3}}{2}d \sin \theta \sin \phi} e^{+ik\frac{d}{2} \cos \theta} + \right. \\ & \left. + e^{-ik\frac{\sqrt{3}}{2}d \sin \theta \sin \phi} e^{+ik\frac{d}{2} \cos \theta} \right\} - \\ & - \hat{e}_\theta \sin \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} \left\{ e^{-ikd \cos \theta} + e^{+ik\frac{\sqrt{3}}{2}d \sin \theta \sin \phi} e^{+ik\frac{d}{2} \cos \theta} + \right. \\ & \left. + e^{-ik\frac{\sqrt{3}}{2}d \sin \theta \sin \phi} e^{+ik\frac{d}{2} \cos \theta} \right\} \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

si ha:

$$N_{\theta}(\theta, \phi) = -\sin\theta \frac{2 \cos\left(\frac{\pi}{2} \cos\theta\right)}{k} \left\{ e^{-ikd \cos\theta} + 2 \cos\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) e^{+ik \frac{d}{2} \cos\theta} \right\}$$

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4 \cos^2\left(\frac{\pi}{2} \cos\theta\right)}{k^2} \left\{ e^{-ikd \cos\theta} + 2 \cos\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) e^{+ik \frac{d}{2} \cos\theta} \right\} \cdot \left\{ e^{+ikd \cos\theta} + 2 \cos\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) e^{-ik \frac{d}{2} \cos\theta} \right\}$$

In definitiva:

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4 \cos^2\left(\frac{\pi}{2} \cos\theta\right)}{k^2} \left\{ 1 + 2 \cos\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) e^{-ik \frac{3}{2} d \cos\theta} + \right. \\ \left. + 2 \cos\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) e^{+ik \frac{3}{2} d \cos\theta} + 4 \cos^2\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) \right\}$$

e, ancora:

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4 \cos^2\left(\frac{\pi}{2} \cos\theta\right)}{k^2} \left\{ 1 + 4 \cos\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) \cos\left(k \frac{3}{2} d \cos\theta\right) + \right. \\ \left. + 4 \cos^2\left(k \frac{\sqrt{3}}{2} d \sin\theta \sin\phi\right) \right\}$$

**11-2) Esercizio n. 2 del 4/2/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\theta = 90^\circ$ . Si ponga  $d = \frac{3}{4}\lambda$ .

Per  $\theta = 90^\circ$  si ha:

$$|N_\theta(\theta, \phi)|_{\theta=90^\circ}^2 = \frac{4}{k^2} \left\{ 1 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \phi \right) + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \phi \right) \right\}$$

$$\langle \vec{S} \rangle_{\theta=90^\circ} = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|_{\theta=90^\circ}^2 + |N_\phi|_{\theta=90^\circ}^2 \right) \hat{e}_r =$$

$$= \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 \left\{ 1 + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \phi \right) \right\}^2 \hat{e}_r$$

Grafichiamo il fattore di forma:

$$F(\phi) = \left\{ 1 + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \phi \right) \right\}^2$$

Poniamo  $d = \frac{3}{4}\lambda$  (come in figura):

$$F(\phi) = \left\{ 1 + 2 \cos \left( \frac{3\sqrt{3}}{4} \pi \sin \phi \right) \right\}^2$$

La funzione  $F(\phi)$  si annulla per:

$$\cos \left( \frac{3\sqrt{3}}{4} \pi \sin \phi_0 \right) = -\frac{1}{2}$$

ossia:

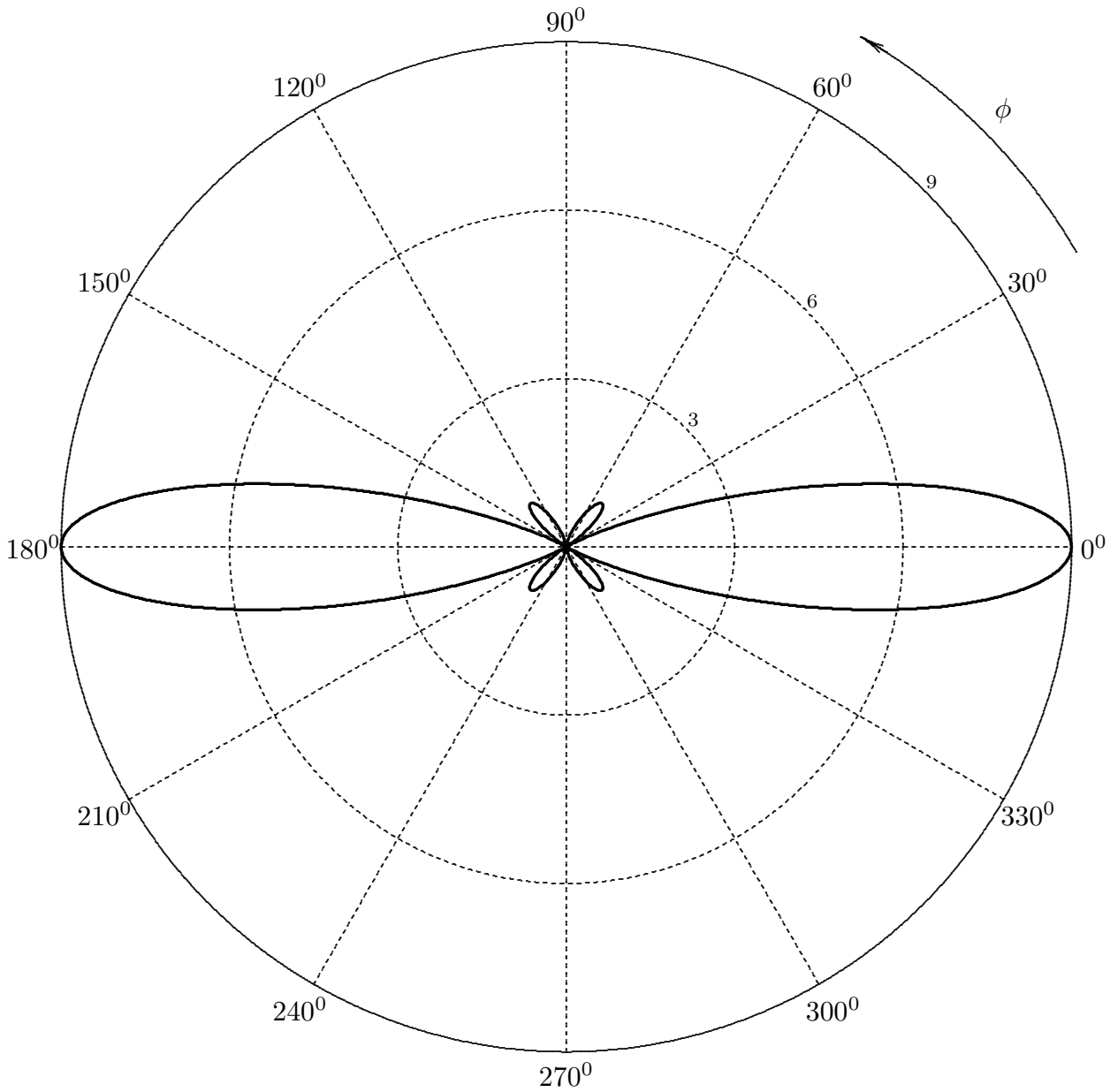
$$\frac{3\sqrt{3}}{4} \pi \sin \phi_0 = \arccos(-0.5) \simeq 2.0944$$

Ne segue:

$$\sin \phi_0 \simeq \frac{4}{3\sqrt{3}\pi} 2.0944 = 0.5132$$

ossia, nel primo quadrante:

$$\phi_0 = \arcsin(0.5132) \simeq 0.5389 \text{ rad} = \underline{\underline{30^\circ.88}}$$



$\phi$	$F(\phi)$	$\phi$	$F(\phi)$	$\phi$	$F(\phi)$	$\phi$	$F(\phi)$
$0^\circ$	9	$5^\circ$	8.2646	$10^\circ$	6.3426	$15^\circ$	3.9373
$20^\circ$	1.8177	$25^\circ$	0.4807	$30^\circ$	0.0090	$35^\circ$	0.1539
$40^\circ$	0.5436	$45^\circ$	0.8740	$50^\circ$	0.9995	$55^\circ$	0.9208
$60^\circ$	0.7187	$65^\circ$	0.4866	$70^\circ$	0.2897	$75^\circ$	0.1543
$80^\circ$	0.0774	$85^\circ$	0.0422	$90^\circ$	0.0326	$95^\circ$	0.0422
$100^\circ$	0.0774	$105^\circ$	0.1543	$110^\circ$	0.2897	$115^\circ$	0.4866
$120^\circ$	0.7187	$125^\circ$	0.9208	$130^\circ$	0.9995	$135^\circ$	0.8740
$140^\circ$	0.5436	$145^\circ$	0.1539	$150^\circ$	0.0090	$155^\circ$	0.4807
$160^\circ$	1.8177	$165^\circ$	3.9373	$170^\circ$	6.3426	$175^\circ$	8.2646
$180^\circ$	9	$185^\circ$	8.2646	$190^\circ$	6.3426	$195^\circ$	3.9373
$200^\circ$	1.8177	$205^\circ$	0.4807	$210^\circ$	0.0090	$215^\circ$	0.1539

220 <sup>0</sup>	0.5436	225 <sup>0</sup>	0.8740	230 <sup>0</sup>	0.9995	235 <sup>0</sup>	0.9208
240 <sup>0</sup>	0.7187	245 <sup>0</sup>	0.4866	250 <sup>0</sup>	0.2897	255 <sup>0</sup>	0.1543
260 <sup>0</sup>	0.0774	265 <sup>0</sup>	0.0422	270 <sup>0</sup>	0.0326	275 <sup>0</sup>	0.0422
280 <sup>0</sup>	0.0774	285 <sup>0</sup>	0.1543	290 <sup>0</sup>	0.2897	295 <sup>0</sup>	0.4866
300 <sup>0</sup>	0.7187	305 <sup>0</sup>	0.9208	310 <sup>0</sup>	0.9995	315 <sup>0</sup>	0.8740
320 <sup>0</sup>	0.5436	325 <sup>0</sup>	0.1539	330 <sup>0</sup>	0.0090	335 <sup>0</sup>	0.4807
340 <sup>0</sup>	1.8176	345 <sup>0</sup>	3.9373	350 <sup>0</sup>	6.3426	355 <sup>0</sup>	8.2645
360 <sup>0</sup>	9						

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Si faccia attenzione che il grafico non si annulla per  $\phi = 90^0$  e  $\phi = 270^0$ .

**11-3) Esercizio n. 3 del 4/2/2011**

Un'onda elettromagnetica piana di frequenza  $\nu = 3 \text{ GHz}$ , viaggiante in aria, penetra, dentro una pozzanghera d'acqua orizzontale, profonda  $d = 1 \text{ cm}$ , lungo la direzione della normale alla superficie dell'acqua. Il fondo della pozzanghera é costituito di cemento il cui indice di rifrazione (trascurando la parte immaginaria) é  $n_3 = 2.2$ . I parametri costitutivi dell'acqua competenti alla frequenza data sono:

$$n_r = 8.743, \quad n_i = 0.6409, \quad \mu = \mu_0.$$

Calcolare il coefficiente di riflessione.

Il sistema puó essere considerato come una lamina piana assorbente (acqua) posta fra l'aria ed il cemento.

Dalla teoria delle lamine piane assorbenti si deduce che il coefficiente di riflessione é:

$$R = \frac{|r_{12}|^2 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}^* r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}^* r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12} r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12} r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Cominciamo con il calcolare alcune quantità che servono per la valutazione dei coefficienti che figurano nella formula della riflettività.:

$$\begin{aligned} (n_1 - n_r) &= (1 - 8.743) = -7.743; & (n_1 + n_r) &= (1 + 8.743) = 9.743 \\ (n_r - n_3) &= (8.743 - 2.2) = 6.543; & (n_r + n_3) &= (8.743 + 2.2) = 10.943 \\ (n_1 - n_r)(n_r - n_3) &\simeq -50.6624; & (n_1 + n_r)(n_r + n_3) &\simeq 106.6176 \\ (n_1 - n_r)(n_r - n_3) - n_i^2 &\simeq -50.6624 - (0.6409)^2 \simeq -51.0731 \\ (n_1 - n_r)(n_r - n_3) + n_i^2 &\simeq -50.6624 + (0.6409)^2 \simeq -50.2517 \\ (n_1 + n_r)(n_r + n_3) - n_i^2 &\simeq 106.6176 - (0.6409)^2 \simeq 106.2069 \\ (n_1 + n_r)(n_r + n_3) + n_i^2 &\simeq 106.6176 + (0.6409)^2 \simeq 107.0284 \end{aligned}$$

Continuiamo con il dimostrare che i denominatori delle quantità  $\Re(r_{12}^* r_{23})$  e  $\Re(r_{12} r_{23})$  sono eguali. Infatti, il denominatore di  $\Re(r_{12}^* r_{23})$  si puó scrivere:

$$\begin{aligned} &[(n_1 + n_r)(n_r + n_3) + n_i^2]^2 + n_i^2(n_3 - n_1)^2 = \\ &= [(n_1 + n_r)(n_r + n_3) + n_i^2]^2 + n_i^2 [(n_3 + n_r) - (n_r + n_1)]^2 = \\ &= [(n_1 + n_r)(n_r + n_3) + n_i^2]^2 + n_i^2(n_3 + n_r)^2 + n_i^2(n_r + n_1)^2 - 2n_i^2(n_3 + n_r)(n_r + n_1) = \\ &= (n_1 + n_r)^2(n_r + n_3)^2 + n_i^4 + n_i^2(n_3 + n_r)^2 + n_i^2(n_r + n_1)^2 = \\ &= (n_1 + n_r)^2 [(n_r + n_3)^2 + n_i^2] + n_i^2 [(n_3 + n_r)^2 + n_i^2] = \\ &= [(n_r + n_1)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2] = 11455.670278 \end{aligned}$$



Allo stesso modo il denominatore di  $\Re(r_{12}r_{23})$  si può scrivere:

$$\begin{aligned}
 & [(n_1 + n_r)(n_r + n_3) - n_i^2]^2 + n_i^2(n_1 + 2n_r + n_3)^2 = \\
 & = [(n_1 + n_r)(n_r + n_3) - n_i^2]^2 + n_i^2 [(n_1 + n_r) + (n_r + n_3)]^2 = \\
 & = [(n_1 + n_r)(n_r + n_3) - n_i^2]^2 + n_i^2(n_3 + n_r)^2 + n_i^2(n_r + n_1)^2 + 2n_i^2(n_3 + n_r)(n_r + n_1) = \\
 & = (n_1 + n_r)^2(n_r + n_3)^2 + n_i^4 + n_i^2(n_3 + n_r)^2 + n_i^2(n_r + n_1)^2 = \\
 & = (n_1 + n_r)^2 [(n_r + n_3)^2 + n_i^2] + n_i^2 [(n_3 + n_r)^2 + n_i^2] = \\
 & = [(n_r + n_1)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2] = 11455.670278
 \end{aligned}$$

$$\begin{aligned}
 \Re(r_{12}^*r_{23}) & = \frac{[(n_1 - n_r)(n_r - n_3) - n_i^2] [(n_1 + n_r)(n_r + n_3) + n_i^2] + n_i^2(n_3 - n_1)^2}{[(n_1 + n_r)(n_r + n_3) + n_i^2]^2 + n_i^2(n_3 - n_1)^2} = \\
 & = \frac{(-51.0731)(107.0283) + (0.6409)^2(1.2)^2}{11455.670278} \simeq -\frac{5465.6755}{11455.670278} \simeq -0.477115
 \end{aligned}$$

$$\begin{aligned}
 \Im(r_{12}^*r_{23}) & = -\frac{2n_i(n_3 - n_1)(n_1n_3 + n_r^2 + n_i^2)}{[(n_1 + n_r)(n_r + n_3) + n_i^2]^2 + n_i^2(n_3 - n_1)^2} = \\
 & = -\frac{2 \cdot 0.6409 \cdot 1.2 \cdot (2.2 + 76.4400 + 0.4107)}{11455.670278} \simeq -\frac{121.5926}{11455.670278} \simeq -0.010614
 \end{aligned}$$

Analogamente:

$$\begin{aligned}
 \Re(r_{12}r_{23}) & = \\
 & = \frac{[(n_1 - n_r)(n_r - n_3) + n_i^2][(n_1 + n_r)(n_r + n_3) - n_i^2] + n_i^2(n_1 - 2n_r + n_3)(n_1 + 2n_r + n_3)}{[(n_1 + n_r)(n_r + n_3) - n_i^2]^2 + n_i^2(n_1 + 2n_r + n_3)^2} = \\
 & = \frac{(-50.2517)(106.2069) + (0.6409)^2(1 - 17.486 + 2.2)(1 + 17.486 + 2.2)}{11455.670278} \simeq \\
 & \simeq \frac{(-5337.0722) + (0.6409)^2(-14.286)(20.686)}{11455.670278} \simeq -\frac{5458.4630}{11455.670278} \simeq -0.476486
 \end{aligned}$$

$$\begin{aligned}
 \Im(r_{12}r_{23}) & = \\
 & = \frac{n_i(n_1 - 2n_r + n_3)[(n_1 + n_r)(n_r + n_3) - n_i^2] - n_i(n_1 + 2n_r + n_3)[(n_1 - n_r)(n_r - n_3) + n_i^2]}{[(n_1 + n_r)(n_r + n_3) - n_i^2]^2 + n_i^2(n_1 + 2n_r + n_3)^2} = \\
 & = \frac{(0.6409)(-14.286)(106.2069) - (0.6409)(20.686)(-50.2517)}{11455.670278} \simeq \\
 & \simeq -\frac{306.199657}{11455.670278} \simeq -0.026729
 \end{aligned}$$

Inoltre:

$$\Re(r_{12}) = \frac{n_1^2 - n_r^2 - n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{75.8508}{95.3368} \simeq -0.795609$$

$$\Re(r_{23}) = \frac{n_r^2 - n_3^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{72.0108}{120.1600} \simeq +0.5993$$

$$\Im(r_{12}) = \frac{-2n_i n_1}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{1.2818}{95.3368} \simeq -0.0134496$$

$$\Im(r_{23}) = \frac{2n_i n_3}{(n_r + n_3)^2 + n_i^2} \simeq \frac{2.81996}{120.1600} \simeq +0.023468$$

$$|r_{12}|^2 = \frac{(n_1 - n_r)^2 + n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq \frac{60.3648}{95.3368} \simeq +0.6332$$

$$|r_{23}|^2 = \frac{(n_r - n_3)^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{43.2216}{120.1600} \simeq +0.3597$$

$$\sin\left(4\pi n_r \frac{d}{\lambda_0}\right) = \sin\left(4\pi \cdot 8.743 \frac{10^{-2} \cdot 3 \cdot 10^9}{3 \cdot 10^8}\right) \simeq \sin(10.9868) \simeq -0.9999615$$

$$\cos\left(4\pi n_r \frac{d}{\lambda_0}\right) = \sin\left(4\pi \cdot 8.743 \frac{10^{-2} \cdot 3 \cdot 10^9}{3 \cdot 10^8}\right) \simeq \cos(10.9868) \simeq -0.008774$$

$$\exp\left[-\left(4\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp\left[-\left(4\pi \cdot 0.6409 \frac{10^{-2} \cdot 3 \cdot 10^9}{3 \cdot 10^8}\right)\right] = \exp(-0.805379) = 0.446918$$

$$\exp\left[-\left(8\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp\left[-\left(8\pi \cdot 0.6409 \frac{10^{-2} \cdot 3 \cdot 10^9}{3 \cdot 10^8}\right)\right] = \exp(-1.610757) = 0.1997364$$

Quindi:

$$R = \frac{0.6332 + 0.446918 [2(-0.477115) \cdot (-0.008774) - 2 \cdot 0.010614 \cdot 0.9999615] + 0.071845}{1 + 0.446918 [2(-0.476486)(-0.008774) - 2(-0.026728)(-0.9999615)] + 0.0454924} \simeq$$

$$\simeq \frac{0.6993}{1.0253397} \simeq \underline{\underline{0.6820 \simeq 68.2\%}}$$

**11-4) Esercizio n. 4 del 4/2/2011**

Con riferimento al problema precedente si valuti il coefficiente di trasmissione.

Poiché risulta, in questo caso:

$$\frac{\beta_3 \mu_1}{\beta_1 \mu_3} = \frac{n_3}{n_1}$$

il coefficiente di trasmissione é:

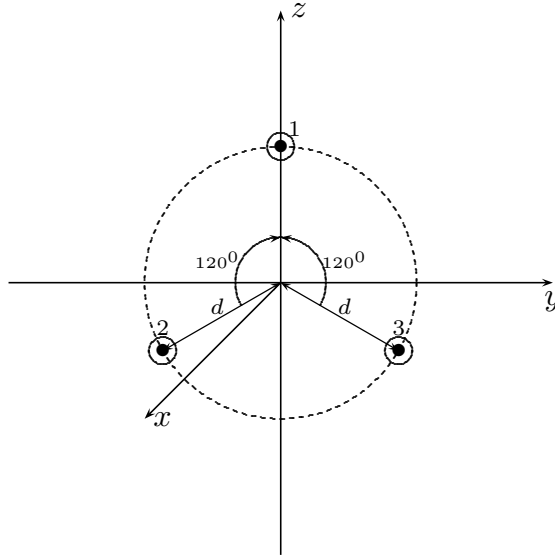
$$T = \frac{\frac{n_3}{n_1} [1 + 2\Re(r_{12}) + |r_{12}|^2] [1 + 2\Re(r_{23}) + |r_{23}|^2] e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Poiché il coefficiente di trasmissione ha lo stesso denominatore del coefficiente di riflessione, procediamo al calcolo del solo numeratore. Si ha:

$$T = \frac{2.2 [1 - 2 \cdot 0.795609 + 0.6332] [1 + 2 \cdot 0.5993 + 0.3597] 0.446918}{1.0253397} \simeq \frac{0.1056}{1.0253397} \simeq \underline{\underline{\simeq 0.10299 \simeq 10.3\%}}$$

**11-5) Esercizio n. 1 del 4/3/2011**

Sia dato un sistema di 3 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate con i loro centri nel piano  $yz$ , con le correnti dirette lungo la direzione dell'asse  $x$ , come in figura. Determinare l'espressione del vettore di Poynting irradiato.



(vedi es. n.1 del 22/9/2003 e es. n.1 del 4/2/2011)

Le densità di corrente sull'antenna 1, sull'antenna 2 e sull'antenna 3 sono rispettivamente:

$$\begin{cases} \vec{J}^{(1)} = \hat{x}A_1\delta(y)\delta(z - z_1)\cos kx & -l \leq x \leq +l \\ \vec{J}^{(2)} = \hat{x}A_2\delta(y - y_2)\delta(z - z_2)\cos kx & -l \leq x \leq +l \\ \vec{J}^{(3)} = \hat{x}A_3\delta(y - y_3)\delta(z - z_3)\cos kx & -l \leq x \leq +l \end{cases}$$

Posto  $A_1 = A_2 = A_3 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante é la somma delle tre:

$$\vec{J} = \hat{x}\delta(y)\delta(z - z_1)\cos kx + \hat{x}\delta(y - y_2)\delta(z - z_2)\cos kx + \hat{x}\delta(y - y_3)\delta(z - z_3)\cos kx$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  é:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}')d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \\ &= \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z' - z_1) \cos kx' dx' dy' dz' + \\ &+ \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_2) \delta(z' - z_2) \cos kx' dx' dy' dz' + \\ &+ \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_3) \delta(z' - z_3) \cos kx' dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \hat{x} e^{-ikz_1 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ &+ \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ &+ \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' \end{aligned}$$

Si ha:

$$\hat{x} \cdot \hat{r} = \cos \psi = \sin \theta \cos \phi$$

essendo  $\psi$  l'angolo formato fra l'asse  $x$  e la direzione del vettore posizione  $\hat{e}_r$ .

Per un'antenna a mezz'onda, orientata secondo l'asse  $x$ , risulta, quindi:

$$\int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' = \int_{-l}^{+l} e^{-ikx' \cos \psi} \cos kx' dx' = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \hat{x} e^{-ikz_1 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} + \\ &+ \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} + \\ &+ \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \end{aligned}$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikz_1 \cos \theta} + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + \right. \\ & \left. + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \right\} + \\ & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikz_1 \cos \theta} + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + \right. \\ & \left. + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \right\} - \\ & - \hat{e}_\phi \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikz_1 \cos \theta} + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + \right. \\ & \left. + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \right\} \end{aligned}$$

Dalla figura risulta:

$$\begin{aligned} z_1 = +d, \quad y_2 = -d \cos(30^\circ) = -\frac{\sqrt{3}}{2}d, \quad z_2 = -d \sin(30^\circ) = -\frac{d}{2}, \\ y_3 = +d \cos(30^\circ) = +\frac{\sqrt{3}}{2}d, \quad z_3 = -d \sin(30^\circ) = -\frac{d}{2} \end{aligned}$$

Quindi:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + e^{+ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta \right. \\
 & \left. + e^{-ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta \right\} + \\
 & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + e^{+ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta \right. \\
 & \left. + e^{-ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta \right\} - \\
 & - \hat{e}_\phi \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + e^{+ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta \right. \\
 & \left. + e^{-ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta \right\}
 \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

Si ha:

$$\begin{aligned}
 N_\theta(\theta, \phi) = & \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + \right. \\
 & \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} \right\}
 \end{aligned}$$

$$\begin{aligned}
 N_\phi(\theta, \phi) = & - \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + \right. \\
 & \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} \right\}
 \end{aligned}$$

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \left\{ e^{-ikd \cos \theta} + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} \right\} \cdot \left\{ e^{+ikd \cos \theta} + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \frac{d}{2} \cos \theta} \right\}$$

$$|N_{\phi}(\theta, \phi)|^2 = \frac{4}{k^2} \sin^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \left\{ e^{-ikd \cos \theta} + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} \right\} \cdot \left\{ e^{+ikd \cos \theta} + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \frac{d}{2} \cos \theta} \right\}$$

In definitiva:

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \left\{ 1 + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \left( \frac{3}{2} \right) d \cos \theta} + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \left( \frac{3}{2} \right) d \cos \theta} + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \right\}$$

$$|N_{\phi}(\theta, \phi)|^2 = \frac{4}{k^2} \sin^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \left\{ 1 + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \left( \frac{3}{2} \right) d \cos \theta} + \right. \\ \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \left( \frac{3}{2} \right) d \cos \theta} + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \right\}$$



e, ancora:

$$\begin{aligned}
 |N_\theta(\theta, \phi)|^2 = & \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{\left( 1 - \sin^2 \theta \cos^2 \phi \right)^2} \left\{ 1 + \right. \\
 & + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + \\
 & \left. + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \right\}
 \end{aligned}$$

$$\begin{aligned}
 |N_\phi(\theta, \phi)|^2 = & \frac{4}{k^2} \sin^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{\left( 1 - \sin^2 \theta \cos^2 \phi \right)^2} \left\{ 1 + \right. \\
 & + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + \\
 & \left. + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \right\}
 \end{aligned}$$

**11-6) Esercizio n. 2 del 4/3/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 0^0$ . Si ponga  $d = \frac{3}{4}\lambda$ .

Per  $\phi = 0^0$  si ha:

$$|N_{\theta}(\theta, \phi)|_{\phi=0^0}^2 = \frac{4}{k^2} \cos^2 \theta \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \right)}{(1 - \sin^2 \theta)^2} \left\{ 1 + 4 \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + 4 \right\}$$

$$|N_{\phi}(\theta, \phi)|_{\phi=0^0}^2 = 0$$

ossia:

$$|N_{\theta}(\theta, \phi)|_{\phi=0^0}^2 = \frac{4}{k^2} \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \right)}{\cos^2 \theta} \left\{ 5 + 4 \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] \right\}$$

$$|N_{\phi}(\theta, \phi)|_{\phi=0^0}^2 = 0$$

Grafichiamo il fattore di forma:

$$[F(\theta)]_{(\phi=0^0)} = \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \right)}{\cos^2 \theta} \left\{ 5 + 4 \cos \left[ kd \left( \frac{3}{2} \right) \cos \theta \right] \right\}$$

Poniamo  $d = \frac{3}{4}\lambda$ ,  $\implies kd = \frac{3}{2}\pi$ .

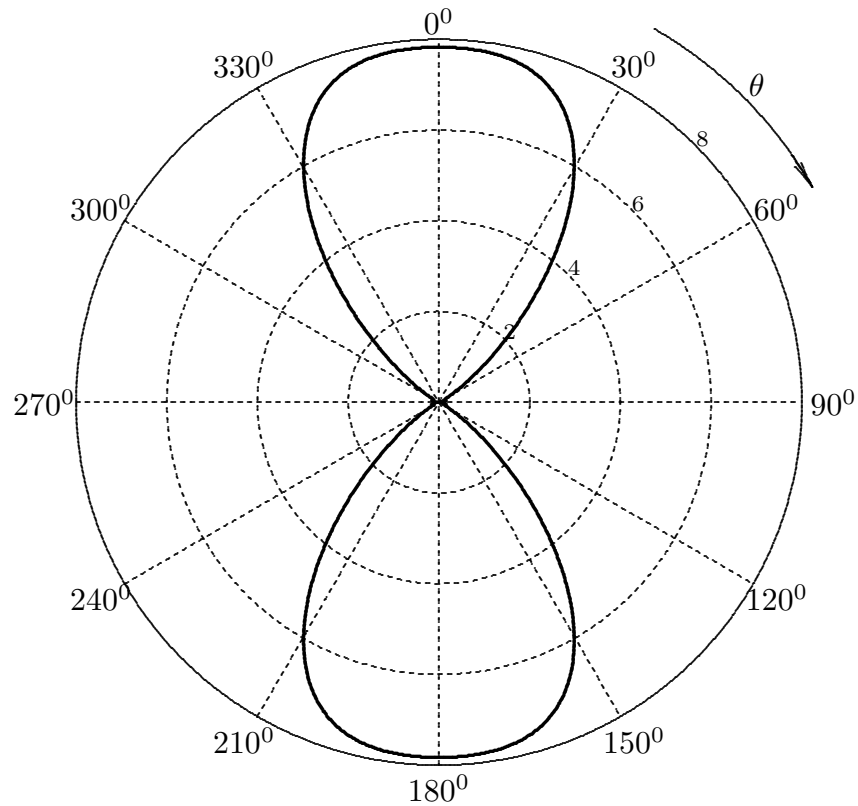
$$[F(\theta)]_{(\phi=0^0)} = \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \right)}{\cos^2 \theta} \left\{ 5 + 4 \cos \left[ \frac{3}{2}\pi \left( \frac{3}{2} \right) \cos \theta \right] \right\}$$

Si ha:

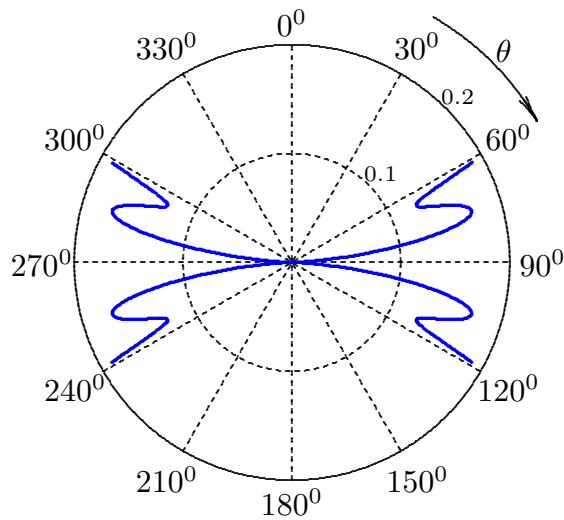
$$\lim_{\theta=90^0} \frac{\cos \left( \frac{\pi}{2} \sin \theta \right)}{\cos \theta} = 0$$

Pertanto la funzione  $F(\theta)$  si annulla per  $\theta = 90^\circ$ .

**Diagramma di radiazione per  $\phi = 0^\circ$**



**Ingrandimento del diagramma in prossimit  dello zero**



$\theta$	$F(\theta)$	$\theta$	$F(\theta)$	$\theta$	$F(\theta)$	$\theta$	$F(\theta)$
$0^\circ$	7.8284	$5^\circ$	7.8156	$10^\circ$	7.7603	$15^\circ$	7.6146
$20^\circ$	7.3095	$25^\circ$	6.7744	$30^\circ$	5.9653	$35^\circ$	4.8964

40°	3.6596	45°	2.4162	50°	1.3521	55°	0.6098
60°	0.2277	65°	0.1261	70°	0.1532	75°	0.1699
80°	0.1198	85°	0.0389	90°	0	95°	0.0389
100°	0.1198	105°	0.1699	110°	0.1532	115°	0.1261
120°	0.2277	125°	0.6098	130°	1.3521	135°	2.4162
140°	3.6596	145°	4.8964	150°	5.9653	155°	6.7744
160°	7.3095	165°	7.6146	170°	7.7603	175°	7.8156
180°	7.8284	185°	7.8156	190°	7.7603	195°	7.6146
200°	7.3095	205°	6.7744	210°	5.9653	215°	4.8964
220°	3.6596	225°	2.4162	230°	1.3521	235°	0.6098
240°	0.2277	245°	0.1261	250°	0.1532	255°	0.1699
260°	0.1198	265°	0.0389	270°	0	275°	0.0389
280°	0.1198	285°	0.1699	290°	0.1532	295°	0.1261
300°	0.2277	305°	0.6098	310°	1.3521	315°	2.4162
320°	3.6596	325°	4.8964	330°	5.9653	335°	6.7744
340°	7.3095	345°	7.6146	350°	7.7603	355°	7.8156
360°	7.8284						

Vogliamo considerare, ora, il diagramma di radiazione per  $\phi = 90^\circ$ .

$$|N_\theta(\theta, \phi)|_{\phi=90^\circ}^2 = 0$$

$$|N_\phi(\theta, \phi)|_{\phi=90^\circ}^2 = \frac{4}{k^2} \left\{ 1 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \right\}$$

$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=0^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \frac{4}{k^2} \left\{ 1 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \right\} \end{aligned}$$

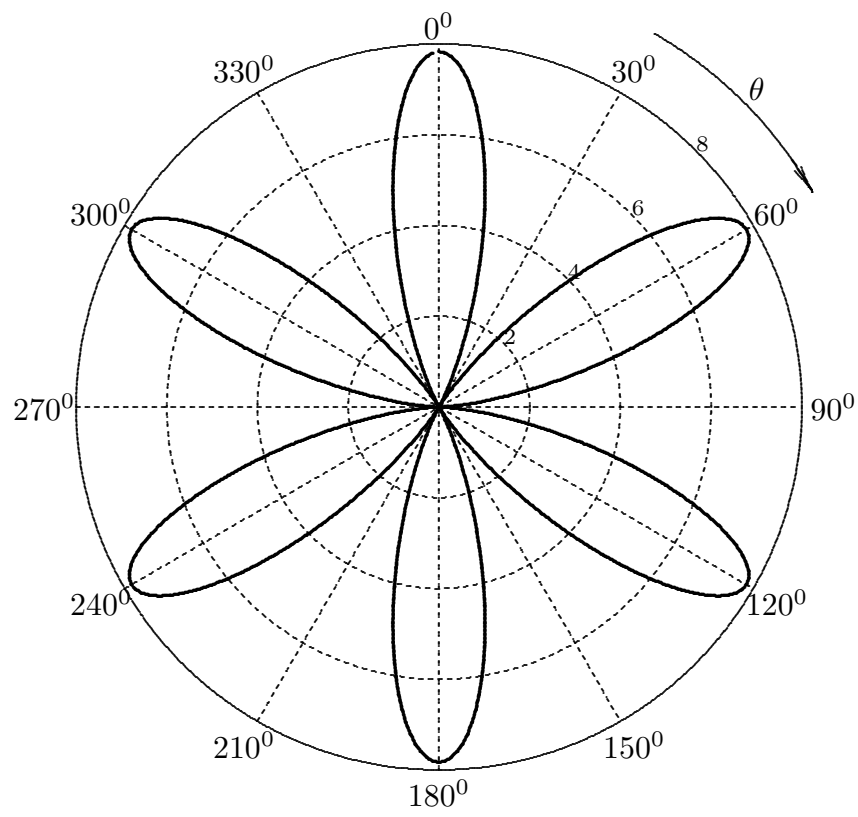
ossia:

$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=0^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 \left\{ 1 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \right\} \end{aligned}$$

Grafichiamo il fattore di forma:

$$F(\theta)_{(\phi=90^\circ)} = \left\{ 1 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left[ k \left( \frac{3}{2} \right) d \cos \theta \right] + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \right\}$$

**Diagramma di radiazione per  $\phi = 90^\circ$**



**11-7) Esercizio n. 3 del 4/3/2011**

Un'onda elettromagnetica piana di frequenza  $\nu = 1 \text{ KHz}$ , viaggiante in aria, incide, in direzione della normale, su una superficie di acqua salmastra che ricopre uno strato di sabbia. I parametri costitutivi dell'acqua salmastra relativi alla frequenza data, sono:

$$\epsilon_r \simeq 80, \quad \sigma \simeq 1 \text{ S/m}, \quad \mu \simeq \mu_0$$

L'indice di rifrazione della sabbia bagnata (trascurando la parte immaginaria) é  $n_3 \simeq 5.4$ .

Se la profondità dell'acqua é  $d = 10 \text{ cm}$ , calcolare il coefficiente di riflessione.

Scriviamo le formule che legano gli indici di rifrazione ai parametri costitutivi dei tre mezzi, attraverso le costanti di propagazione  $\beta$  ed i coefficienti di attenuazione  $\alpha$  dell'onda elettromagnetica:

$$\beta_1 = \frac{\omega}{c} n_1, \quad \beta_2 = \frac{\omega}{c} \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ 1 + \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} \right]} = \frac{\omega}{c} n_r,$$

$$\alpha_2 = \frac{\omega}{c} \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} - 1 \right]} = \frac{\omega}{c} n_i, \quad \beta_3 = \frac{\omega}{c} n_3$$

Poiché il primo mezzo é l'aria, risulta  $n_1 = 1$ . Per il secondo mezzo, si ha:

$$n_r = \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ 1 + \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} \right]}, \quad n_i = \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} - 1 \right]}$$

Si ha:

$$\frac{\sigma^2}{\epsilon_2^2 \omega^2} = \frac{1}{(8.854 \cdot 10^{-12} \cdot 80 \cdot 2\pi \cdot 10^3)^2} \simeq 5.05 \cdot 10^{10} \gg 1$$

ossia:

$$\left[ 1 + \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} \right] \simeq \left[ \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} - 1 \right] \simeq \sqrt{\frac{\sigma^2}{\epsilon_2^2 \omega^2}} \simeq 2.2472 \cdot 10^5$$

per cui si può approssimare:

$$n_r = n_i \simeq \sqrt{40 \cdot 2.2472 \cdot 10^5} \simeq 2998$$

Il sistema può essere considerato come una lamina piana assorbente (acqua) posta fra l'aria ed il cemento.

Dalla teoria delle lamine piane assorbenti si deduce che il coefficiente di riflessione é:

$$R = \frac{|r_{12}|^2 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}^* r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}^* r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12} r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12} r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Cominciamo con il calcolare alcune quantità che servono per la valutazione dei coefficienti che figurano nella formula della riflettività.:

$$(n_1 - n_r) = (1 - 2998) = -2997; \quad (n_1 + n_r) = (1 + 2998) = 2999$$

$$(n_r - n_3) = (2998 - 5.4) = 2992.6; \quad (n_r + n_3) = (2998 + 5.4) = 3003.4$$

$$[(n_1 - n_r)(n_1 + n_r) - n_i^2] = -2997 \cdot 2999 - (2998)^2 = -1.7976 \cdot 10^7$$

$$[(n_r - n_3)(n_r + n_3) + n_i^2] = 2992.6 \cdot 3003.4 + (2998)^2 = +1.7976 \cdot 10^7$$

$$[(n_1 + n_r)^2 + n_i^2] = (2999)^2 + (2998)^2 = 1.7982 \cdot 10^7$$

$$[(n_1 - n_r)^2 + n_i^2] = (1 - 2998)^2 + (2998)^2 = 1.797 \cdot 10^7$$

$$[(n_r + n_3)^2 + n_i^2] = (2998 + 5.4)^2 + (2998)^2 = 1.8008 \cdot 10^7$$

$$[(n_r - n_3)^2 + n_i^2] = (2998 - 5.4)^2 + (2998)^2 = 1.7944 \cdot 10^7$$

$$4n_i^2 n_1 n_3 = 4 \cdot (2998)^2 \cdot 5.4 = 1.9414 \cdot 10^8$$

$$\begin{aligned} \Re(r_{12}^* r_{23}) &= \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] - 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{(-1.7976 \cdot 10^7)(+1.7976 \cdot 10^7) - 1.9414 \cdot 10^8}{3.2382 \cdot 10^{14}} \simeq -\frac{3.2314 \cdot 10^{14}}{3.2382 \cdot 10^{14}} \simeq -0.9979 \end{aligned}$$

$$\begin{aligned} \Im(r_{12}^* r_{23}) &= \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] + 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{2 \cdot 2998 \cdot 5.4 \cdot (-1.7976 \cdot 10^7) + 2 \cdot 2998 \cdot (+1.7976 \cdot 10^7)}{3.2382 \cdot 10^{14}} \simeq \\ &\simeq \frac{-5.8203 \cdot 10^{11} + 1.0778 \cdot 10^{11}}{3.2382 \cdot 10^{14}} \simeq -\frac{4.7425 \cdot 10^{11}}{3.2382 \cdot 10^{14}} \simeq -0.0014645 \end{aligned}$$

$$\begin{aligned} \Re(r_{12} r_{23}) &= \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] + 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{(-1.7976 \cdot 10^7)(+1.7976 \cdot 10^7) + 1.9414 \cdot 10^8}{3.2382 \cdot 10^{14}} \simeq -\frac{3.2314 \cdot 10^{14}}{3.2382 \cdot 10^{14}} \simeq -0.9979 \end{aligned}$$

$$\begin{aligned}\Im(r_{12}r_{23}) &= \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] - 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2][(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{2 \cdot 2998 \cdot 5.4 \cdot (-1.7976 \cdot 10^7) - 2 \cdot 2998 \cdot (+1.7976 \cdot 10^7)}{3.2382 \cdot 10^{14}} \simeq \\ &\simeq \frac{-5.8203 \cdot 10^{11} - 1.0778 \cdot 10^{11}}{3.2382 \cdot 10^{14}} \simeq -\frac{6.8981 \cdot 10^{11}}{3.2382 \cdot 10^{14}} \simeq -0.0021302\end{aligned}$$

Inoltre:

$$\begin{aligned}\Re(r_{12}) &= \frac{n_1^2 - n_r^2 - n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{1.7976007 \cdot 10^7}{1.7982005 \cdot 10^7} \simeq -0.9996664443147 \\ \Re(r_{23}) &= \frac{n_r^2 - n_3^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{1.7975978 \cdot 10^7}{1.8008415 \cdot 10^7} \simeq +0.99819878651175 \\ \Im(r_{12}) &= \frac{-2n_i n_1}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{5996}{1.7982005 \cdot 10^7} \simeq -0.0003334444629506 \\ \Im(r_{23}) &= \frac{2n_i n_3}{(n_r + n_3)^2 + n_i^2} \simeq \frac{32378.4}{1.8008415 \cdot 10^7} \simeq +0.00179795945395528 \\ |r_{12}|^2 &= \frac{(n_1 - n_r)^2 + n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq \frac{1.7970013 \cdot 10^7}{1.7982005 \cdot 10^7} \simeq +0.999333111074099 \\ |r_{23}|^2 &= \frac{(n_r - n_3)^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{1.7943658 \cdot 10^7}{1.8008415 \cdot 10^7} \simeq +0.99640406998617\end{aligned}$$

$$\sin\left(4\pi n_r \frac{d}{\lambda_0}\right) = \sin\left(4\pi \cdot 2998 \frac{0.1 \cdot 10^3}{3 \cdot 10^8}\right) \simeq \sin(0.012558) \simeq +0.012558$$

$$\cos\left(4\pi n_r \frac{d}{\lambda_0}\right) = \cos\left(4\pi \cdot 2998 \frac{0.1 \cdot 10^3}{3 \cdot 10^8}\right) \simeq \cos(0.012558) \simeq +0.99992$$

$$\exp\left[-\left(4\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp\left[-\left(4\pi \cdot 2998 \frac{0.1 \cdot 10^3}{3 \cdot 10^8}\right)\right] = \exp(-0.012558) = 0.98752$$

$$\exp\left[-\left(8\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp\left[-\left(8\pi \cdot 2998 \frac{0.1 \cdot 10^3}{3 \cdot 10^8}\right)\right] = \exp(-0.025116) = 0.9752$$

Quindi:

$$\begin{aligned}R &= \frac{0.99933 + 0.98752 [2(-0.9979) \cdot (0.99992) - 2(-0.0014645) \cdot 0.012558] + 0.97174}{1 + 0.98752 [2(-0.9979)(0.99992) - 2(-0.0021302)(0.012558)] + 0.97109} \simeq \\ &\simeq \frac{0.00037158}{0.00040809} \simeq \underline{\underline{0.91053}} \simeq \underline{\underline{91\%}}\end{aligned}$$



**11-8) Esercizio n. 4 del 4/3/2011**

Con riferimento al problema precedente si valuti il coefficiente di trasmissione.

Poiché risulta, in questo caso:

$$\frac{\beta_3 \mu_1}{\beta_1 \mu_3} = \frac{n_3}{n_1}$$

il coefficiente di trasmissione é:

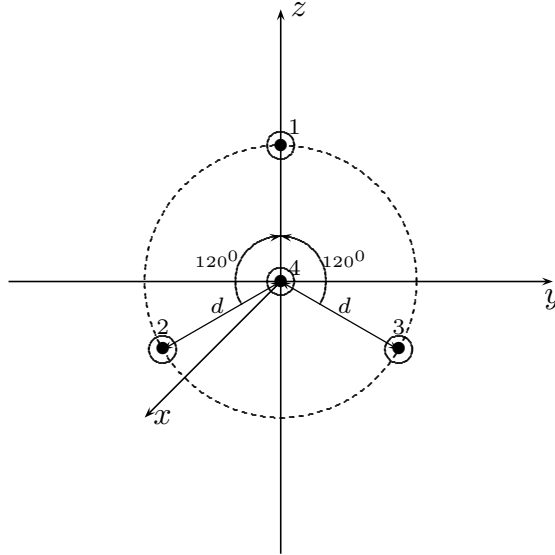
$$T = \frac{\frac{n_3}{n_1} [1 + 2\Re(r_{12}) + |r_{12}|^2] [1 + 2\Re(r_{23}) + |r_{23}|^2] e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)} \right]}$$

Poiché il coefficiente di trasmissione ha lo stesso denominatore del coefficiente di riflessione, procediamo al calcolo del solo numeratore. Si ha:

$$T = 5.4 [1 - 2 \cdot 0.9996664443147 + 0.999333111074099] \cdot \frac{[1 + 2 \cdot 0.99819878651175 + 0.99640406998617] \cdot 0.98752}{0.00040809} \simeq \frac{4.73630275986131 \cdot 10^{-6}}{0.00040809} \simeq \underline{\underline{\simeq 0.0116 \simeq 1.16\%}}$$

**11-9) Esercizio n. 1 del 6/5/2011**

Sia dato un sistema di 4 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate con i loro centri nel piano  $yz$ , con le correnti dirette lungo la direzione dell'asse  $x$ , come in figura. Determinare l'espressione del vettore di Poynting irradiato.



(vedi es. n.1 del 22/9/2003, es. n.1 del 4/2/2011 e es. n.1 del 4/3/2011)

Le densità di corrente sull'antenna 1, sull'antenna 2, sull'antenna 3 e sull'antenna 4 sono rispettivamente:

$$\left\{ \begin{array}{ll} \vec{J}^{(1)} = \hat{x}A_1\delta(y)\delta(z - z_1) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(2)} = \hat{x}A_2\delta(y - y_2)\delta(z - z_2) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(3)} = \hat{x}A_3\delta(y - y_3)\delta(z - z_3) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(4)} = \hat{x}A_4\delta(y)\delta(z) \cos kx & -l \leq x \leq +l \end{array} \right.$$

Posto  $A_1 = A_2 = A_3 = A_4 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante é la somma delle quattro:

$$\vec{J} = \hat{x}\delta(y)\delta(z - z_1) \cos kx + \hat{x}\delta(y - y_2)\delta(z - z_2) \cos kx + \\ + \hat{x}\delta(y - y_3)\delta(z - z_3) \cos kx + \hat{x}\delta(y)\delta(z) \cos kx$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  é:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}') d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z' - z_1) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_2) \delta(z' - z_2) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_3) \delta(z' - z_3) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z') \cos kx' dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{x} e^{-ikz_1 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' \end{aligned}$$

Si ha:

$$\hat{x} \cdot \hat{r} = \cos \psi = \sin \theta \cos \phi$$

essendo  $\psi$  l'angolo formato fra l'asse  $x$  e la direzione del vettore posizione  $\hat{e}_r$ .

Per un'antenna a mezz'onda, orientata secondo l'asse  $x$ , risulta, quindi:

$$\int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' = \int_{-l}^{+l} e^{-ikx' \cos \psi} \cos kx' dx' = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

Ne segue:

$$\begin{aligned}\vec{N}(\theta, \phi) = & \hat{x} e^{-ikz_1} \cos \theta \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} + \\ & + \hat{x} e^{-iky_2} \sin \theta \sin \phi e^{-ikz_2} \cos \theta \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} + \\ & + \hat{x} e^{-iky_3} \sin \theta \sin \phi e^{-ikz_3} \cos \theta \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} + \\ & + \hat{x} \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)}\end{aligned}$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned}\vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left\{ e^{-ikz_1} \cos \theta + e^{-iky_2} \sin \theta \sin \phi e^{-ikz_2} \cos \theta + \right. \\ & \left. + e^{-iky_3} \sin \theta \sin \phi e^{-ikz_3} \cos \theta + 1 \right\} + \\ & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left\{ e^{-ikz_1} \cos \theta + e^{-iky_2} \sin \theta \sin \phi e^{-ikz_2} \cos \theta + \right. \\ & \left. + e^{-iky_3} \sin \theta \sin \phi e^{-ikz_3} \cos \theta + 1 \right\} - \\ & - \hat{e}_\phi \sin \phi \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left\{ e^{-ikz_1} \cos \theta + e^{-iky_2} \sin \theta \sin \phi e^{-ikz_2} \cos \theta + \right. \\ & \left. + e^{-iky_3} \sin \theta \sin \phi e^{-ikz_3} \cos \theta + 1 \right\}\end{aligned}$$

Dalla figura risulta:

$$\begin{aligned}z_1 = +d, \quad y_2 = -d \cos(30^\circ) = -\frac{\sqrt{3}}{2}d, \quad z_2 = -d \sin(30^\circ) = -\frac{d}{2}, \\ y_3 = +d \cos(30^\circ) = +\frac{\sqrt{3}}{2}d, \quad z_3 = -d \sin(30^\circ) = -\frac{d}{2}\end{aligned}$$

Quindi:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + e^{+ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta + \right. \\
 & \left. + e^{-ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta + 1 \right\} + \\
 & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + e^{+ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta + \right. \\
 & \left. + e^{-ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta + 1 \right\} - \\
 & - \hat{e}_\phi \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + e^{+ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta + \right. \\
 & \left. + e^{-ik \frac{\sqrt{3}}{2} d \sin \theta \sin \phi} + ik \frac{d}{2} \cos \theta + 1 \right\}
 \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

Si ha:

$$\begin{aligned}
 N_\theta(\theta, \phi) = & \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + \right. \\
 & \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} + 1 \right\}
 \end{aligned}$$

$$\begin{aligned}
 N_\phi(\theta, \phi) = & - \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-ikd \cos \theta} + \right. \\
 & \left. + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} + 1 \right\}
 \end{aligned}$$

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \cdot \left\{ e^{-ikd \cos \theta} + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} + 1 \right\} \cdot \left\{ e^{+ikd \cos \theta} + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \frac{d}{2} \cos \theta} + 1 \right\}$$

$$|N_{\phi}(\theta, \phi)|^2 = \frac{4}{k^2} \sin^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \cdot \left\{ e^{-ikd \cos \theta} + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} + 1 \right\} \cdot \left\{ e^{+ikd \cos \theta} + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \frac{d}{2} \cos \theta} + 1 \right\}$$

In definitiva:

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \cdot \left\{ 1 + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \left( \frac{3}{2} \right) d \cos \theta} + e^{-ikd \cos \theta} + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \left( \frac{3}{2} \right) d \cos \theta} + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{+ik \frac{d}{2} \cos \theta} + e^{+ikd \cos \theta} + 2 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) e^{-ik \frac{d}{2} \cos \theta} + 1 \right\} = \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{(1 - \sin^2 \theta \cos^2 \phi)^2} \cdot \left\{ 2 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \cos \left( k \frac{3}{2} d \cos \theta \right) + 2 \cos (kd \cos \theta) + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \cos \left( k \frac{d}{2} \cos \theta \right) \right\}$$

par Analogamente:

$$\begin{aligned}
 |N_\phi(\theta, \phi)|^2 &= \frac{4}{k^2} \sin^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{\left( 1 - \sin^2 \theta \cos^2 \phi \right)^2} \cdot \\
 &\cdot \left\{ 2 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \cos \left( \frac{3}{2} kd \cos \theta \right) + 2 \cos (kd \cos \theta) + \right. \\
 &\left. + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \sin \phi \right) \cos \left( k \frac{d}{2} \cos \theta \right) \right\}
 \end{aligned}$$

**11-10) Esercizio n. 2 del 6/5/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 90^\circ$ . Si ponga  $d = \frac{3}{4}\lambda$ .

Si ha:

$$|N_\theta(\theta, \phi)|_{(\phi=90^\circ)}^2 = 0$$

$$|N_\phi(\theta, \phi)|_{(\phi=90^\circ)}^2 = \frac{4}{k^2} \left\{ 2 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left( k \frac{3}{2} d \cos \theta \right) + 2 \cos (kd \cos \theta) + \right. \\ \left. + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left( k \frac{d}{2} \cos \theta \right) \right\}$$

Quindi:

$$\langle \vec{S} \rangle_{(\phi=90^\circ)} = \\ = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \frac{4}{k^2} \left\{ 2 + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left( k \frac{3}{2} d \cos \theta \right) + 2 \cos (kd \cos \theta) + \right. \\ \left. + 4 \cos^2 \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) + 4 \cos \left( k \frac{\sqrt{3}}{2} d \sin \theta \right) \cos \left( k \frac{d}{2} \cos \theta \right) \right\} \hat{e}_r$$

Poniamo  $d = \frac{3}{4}\lambda, \implies kd = \frac{3}{2}\pi$ .

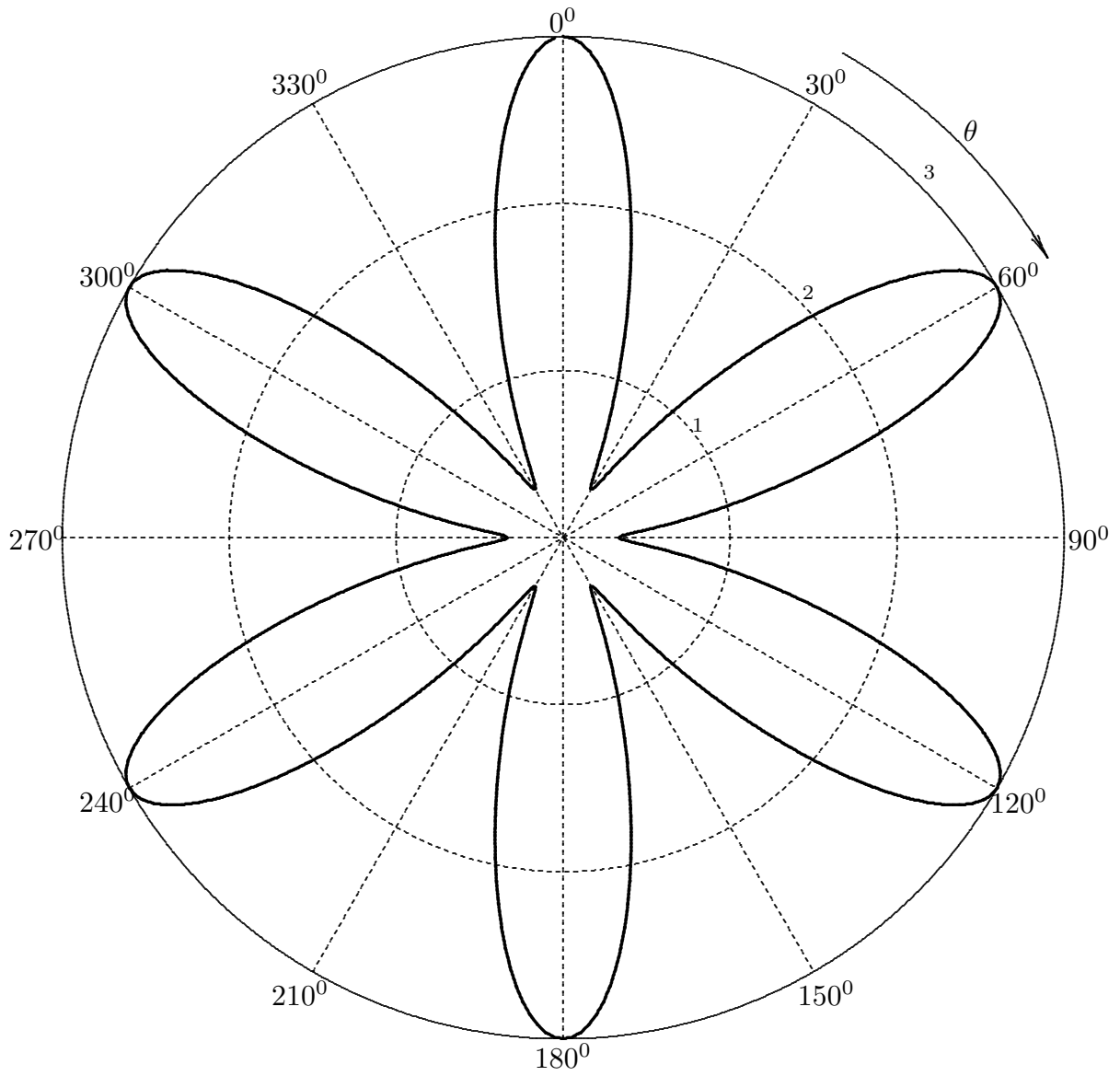
$$\langle \vec{S} \rangle_{(\phi=90^\circ)} = \\ = Z \left( \frac{1}{2\pi r} \right)^2 \left\{ 1 + 2 \cos \left( \frac{3\sqrt{3}}{4} \pi \sin \theta \right) \cos \left( \frac{9}{4} \pi \cos \theta \right) + \cos \left( \frac{3}{2} \pi \cos \theta \right) + \right. \\ \left. + 2 \cos^2 \left( \frac{3\sqrt{3}}{4} \pi \sin \theta \right) + 2 \cos \left( \frac{3\sqrt{3}}{4} \pi \sin \theta \right) \cos \left( \frac{3}{4} \pi \cos \theta \right) \right\} \hat{e}_r$$

Grafichiamo il fattore di forma:

$$[F(\theta)]_{(\phi=90^\circ)} = \left\{ 1 + 2 \cos \left( \frac{3\sqrt{3}}{4} \pi \sin \theta \right) \cos \left( \frac{9}{4} \pi \cos \theta \right) + \cos \left( \frac{3}{2} \pi \cos \theta \right) + \right. \\ \left. + 2 \cos^2 \left( \frac{3\sqrt{3}}{4} \pi \sin \theta \right) + 2 \cos \left( \frac{3\sqrt{3}}{4} \pi \sin \theta \right) \cos \left( \frac{3}{4} \pi \cos \theta \right) \right\}$$



**Diagramma di radiazione per  $\phi = 90^\circ$**



Vogliamo considerare, ora, il diagramma di radiazione per  $\phi = 0^0$ .

$$|N_{\theta}(\theta, \phi)|_{(\phi=0^0)}^2 = \frac{4}{k^2} \frac{\cos^2\left(\frac{\pi}{2} \sin \theta\right)}{\cos^2 \theta} \cdot \left\{ 6 + 4 \cos\left(k \frac{3}{2} d \cos \theta\right) + 2 \cos(kd \cos \theta) + 4 \cos\left(k \frac{d}{2} \cos \theta\right) \right\}$$

$$|N_{\phi}(\theta, \phi)|^2 = 0$$

Quindi:

$$\langle \vec{S} \rangle_{(\phi=0^0)} = \frac{1}{2} Z \left(\frac{k}{4\pi r}\right)^2 \frac{4}{k^2} \frac{\cos^2\left(\frac{\pi}{2} \sin \theta\right)}{\cos^2 \theta} \cdot \left\{ 6 + 4 \cos\left(k \frac{3}{2} d \cos \theta\right) + 2 \cos(kd \cos \theta) + 4 \cos\left(k \frac{d}{2} \cos \theta\right) \right\} \hat{e}_r$$

Poniamo  $d = \frac{3}{4}\lambda$ ,  $\implies kd = \frac{3}{2}\pi$ .

$$\langle \vec{S} \rangle_{(\phi=0^0)} = Z \left(\frac{1}{2\pi r}\right)^2 \frac{\cos^2\left(\frac{\pi}{2} \sin \theta\right)}{\cos^2 \theta} \cdot \left\{ 3 + 2 \cos\left(\frac{9}{4}\pi \cos \theta\right) + \cos\left(\frac{3}{2}\pi \cos \theta\right) + 2 \cos\left(\frac{3}{4}\pi \cos \theta\right) \right\} \hat{e}_r$$

Grafichiamo il fattore di forma:

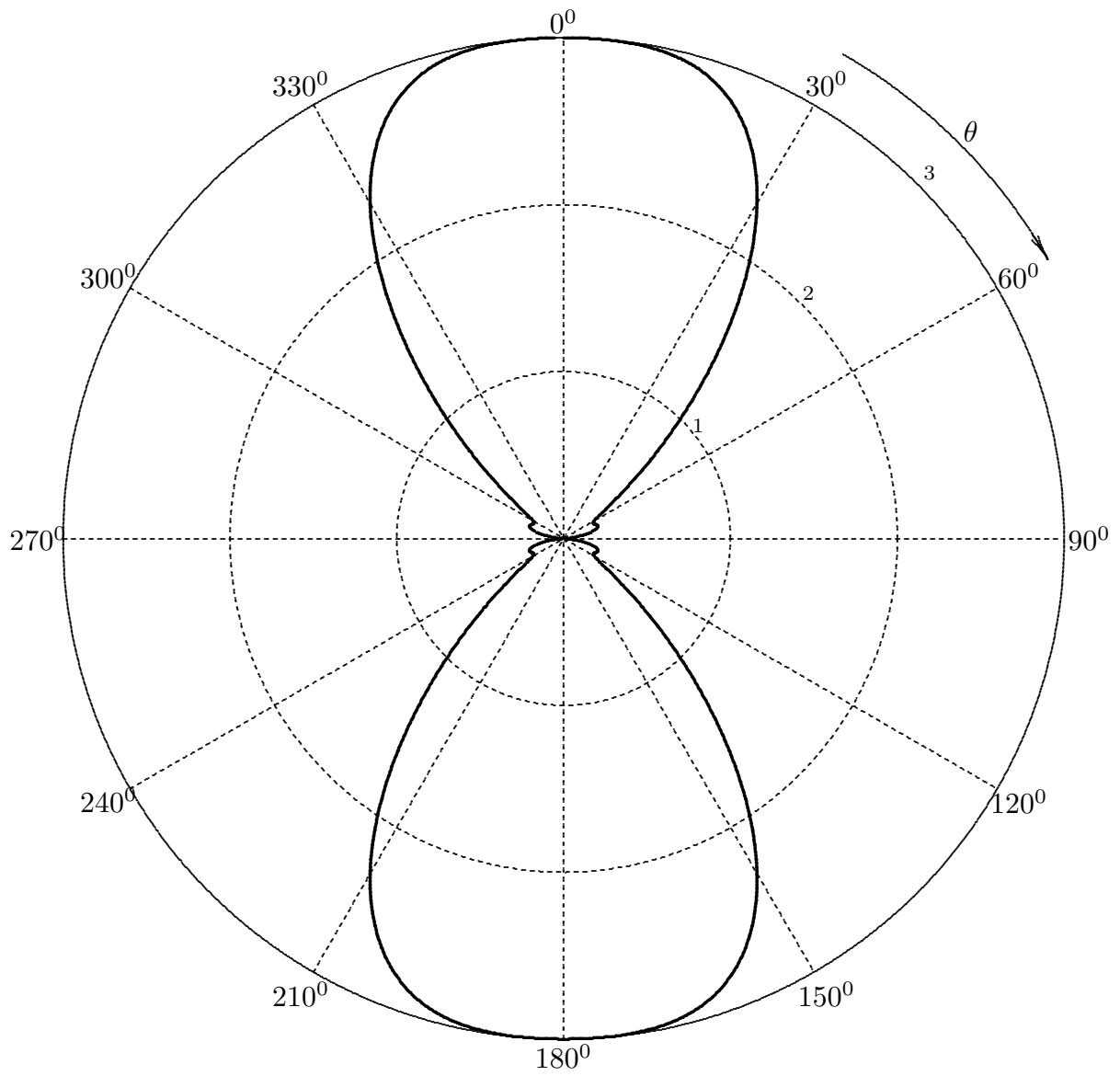
$$[F(\theta)]_{(\phi=0^0)} = \frac{\cos^2\left(\frac{\pi}{2} \sin \theta\right)}{\cos^2 \theta} \left\{ 3 + 2 \cos\left(\frac{9}{4}\pi \cos \theta\right) + \cos\left(\frac{3}{2}\pi \cos \theta\right) + 2 \cos\left(\frac{3}{4}\pi \cos \theta\right) \right\}$$

Si ha:

$$\lim_{\theta=90^0} \frac{\cos\left(\frac{\pi}{2} \sin \theta\right)}{\cos \theta} = 0$$

Pertanto la funzione  $F(\theta)$  si annulla per  $\theta = 90^0$ .

Diagramma di radiazione per  $\phi = 0^\circ$



**11-11) Esercizio n. 3 del 6/5/2011**

Un'onda elettromagnetica piana, di lunghezza d'onda relativa al vuoto  $\lambda_0$ , viaggiante in un mezzo di indice di rifrazione  $n_1 = 1.5$ , incontra la superficie di separazione fra tale mezzo e l'aria. Calcolare l'angolo limite. Se l'angolo di incidenza dell'onda elettromagnetica é compreso fra l'angolo limite e l'angolo di  $90^0$ , esprimere il coefficiente di attenuazione, nonché la profondità di penetrazione in unità di lunghezza d'onda relativa al vuoto, lungo la direzione normale all'interfaccia, nell'aria.

Supponiamo che l'onda elettromagnetica incida sulla superficie di separazione fra il vetro e l'aria (nel caso della luce) o equivalentemente fra la paraffina e l'aria (nel caso di microonde). Si ha allora, per esempio:

$$n_1 = 1.5, n_2 = 1, \theta_L = \arcsin\left(\frac{n_2}{n_1}\right) = \arcsin\left(\frac{1}{1.5}\right) \simeq 0.7297 \text{ rad} \simeq \underline{\underline{41^0.81}}$$

Come sappiamo il coefficiente di attenuazione lungo la normale all'interfaccia nel mezzo meno rifrangente é:

$$\beta_1 = \omega \sqrt{\epsilon_1 \mu_1} \sqrt{\sin^2 \theta_0 - \frac{\epsilon_2}{\epsilon_1}} = \frac{\omega}{c} n_1 \sqrt{\sin^2 \theta_0 - \frac{n_2^2}{n_1^2}} = \frac{2\pi}{\lambda_0} n_1 \sqrt{\sin^2 \theta_0 - \frac{n_2^2}{n_1^2}} \quad (\theta_L < \theta_0 < 90^0)$$

essendo  $\lambda_0$  la lunghezza d'onda, relativa al vuoto, dell'onda incidente.

La profondità di penetrazione dell'onda (superficiale) nel mezzo meno rifrangente (aria) é, allora:

$$\delta = \frac{1}{\beta_1} = \frac{\lambda_0}{2\pi} \frac{1}{n_1 \sqrt{\sin^2 \theta_0 - \frac{n_2^2}{n_1^2}}}$$

che in unità di lunghezza d'onda diventa:

$\frac{\delta}{\lambda_0} = \frac{1}{2\pi n_1 \sqrt{\sin^2 \theta_0 - \frac{n_2^2}{n_1^2}}} \quad (\theta_L < \theta_0 < 90^0)$
---

Essa dipende fortemente dall'angolo di incidenza.

**11-12) Esercizio n. 4 del 6/5/2011**

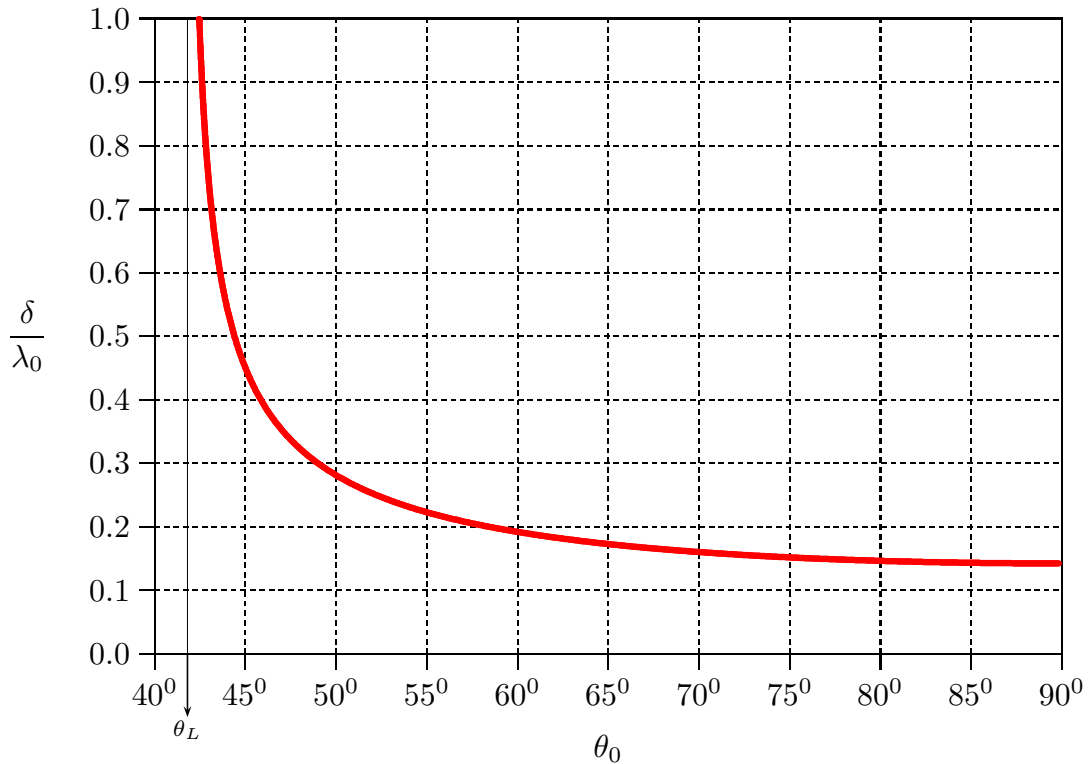
Graficare in funzione di  $\theta_0$  ( $\theta_L < \theta_0 < 90^\circ$ ) la profondità di penetrazione dell'onda superficiale, in unità di lunghezza d'onda relativa al vuoto, nell'aria.

Si ha:

$$\frac{\delta}{\lambda_0} = \frac{1}{2\pi \cdot 1.5 \sqrt{\sin^2 \theta_0 - \frac{1}{(1.5)^2}}} \quad (\theta_L < \theta_0 < 90^\circ)$$

**Profondità di penetrazione dell'onda superficiale  
nel mezzo meno rifrangente**

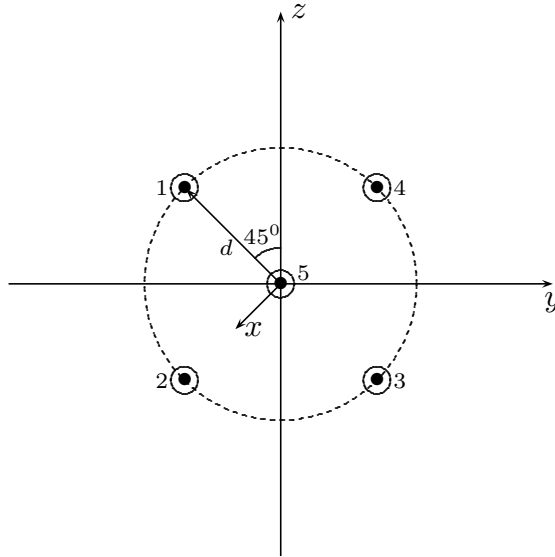
$$\theta_L = 41^\circ.81, \quad n_1 = 1.5, \quad n_2 = 1$$



$\theta_0$	$d/\lambda_0$	$\theta_0$	$d/\lambda_0$	$\theta_0$	$d/\lambda_0$	$\theta_0$	$d/\lambda_0$
$42^\circ$	1.8495	$43^\circ$	0.7378	$44^\circ$	0.5435	$45^\circ$	0.4502
$46^\circ$	0.4927	$47^\circ$	0.3528	$48^\circ$	0.3231	$49^\circ$	0.2999
$50^\circ$	0.2812	$55^\circ$	0.2229	$60^\circ$	0.1919	$65^\circ$	0.1728
$70^\circ$	0.1602	$75^\circ$	0.1518	$80^\circ$	0.1464	$85^\circ$	0.1433

**11-13) Esercizio n. 1 del 1/7/2011**

Sia dato un sistema di 5 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Quattro di esse sono posizionate con i loro centri nel piano  $yz$  ai vertici di un quadrato circoscritto da una circonferenza di raggio  $d$ , la quinta é posizionata con il centro nell'origine delle coordinate. Le correnti sono orientate lungo la direzione dell'asse  $x$ , come in figura. Determinare l'espressione del vettore di Poynting irradiato.



(vedi es. n.1 del 6/5/2011)

Le densità di corrente sull'antenna 1, sull'antenna 2, sull'antenna 3, sull'antenna 4 e sull'antenna 5 sono rispettivamente:

$$\left\{ \begin{array}{ll} \vec{J}^{(1)} = \hat{x} A_1 \delta(y - y_1) \delta(z - z_1) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(2)} = \hat{x} A_2 \delta(y - y_2) \delta(z - z_2) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(3)} = \hat{x} A_3 \delta(y - y_3) \delta(z - z_3) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(4)} = \hat{x} A_4 \delta(y - y_4) \delta(z - z_4) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(5)} = \hat{x} A_5 \delta(y) \delta(z) \cos kx & -l \leq x \leq +l \end{array} \right.$$

Posto  $A_1 = A_2 = A_3 = A_4 = A_5 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante é la somma delle cinque:

$$\vec{J} = \hat{x} \delta(y - y_1) \delta(z - z_1) \cos kx + \hat{x} \delta(y - y_2) \delta(z - z_2) \cos kx + \\ + \hat{x} \delta(y - y_3) \delta(z - z_3) \cos kx + \hat{x} \delta(y - y_4) \delta(z - z_4) \cos kx + \hat{x} \delta(y) \delta(z) \cos kx$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  é:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}') d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_1) \delta(z' - z_1) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_2) \delta(z' - z_2) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_3) \delta(z' - z_3) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_4) \delta(z' - z_4) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z') \cos kx' dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{x} e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' \end{aligned}$$

Si ha:

$$\hat{x} \cdot \hat{r} = \cos \psi = \sin \theta \cos \phi$$

essendo  $\psi$  l'angolo formato fra l'asse  $x$  e la direzione del vettore posizione  $\hat{e}_r$ .

Per un'antenna a mezz'onda, orientata secondo l'asse  $x$ , risulta, quindi:

$$\int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' = \int_{-l}^{+l} e^{-ikx' \cos \psi} \cos kx' dx' = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{x} e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} + \\ & + \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} + \\ & + \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} + \\ & + \hat{x} e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} + \\ & + \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \end{aligned}$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$



si ha:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} + \right. \\
 & + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} + \\
 & \left. + e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} + 1 \right\} + \\
 & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} + \right. \\
 & + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} + \\
 & \left. + e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} + 1 \right\} - \\
 & - \hat{e}_\phi \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} + \right. \\
 & + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} + \\
 & \left. + e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} + 1 \right\}
 \end{aligned}$$

Dalla figura risulta:

$$\left\{ \begin{array}{l} y_1 = -\frac{d}{\sqrt{2}}, \quad z_1 = +\frac{d}{\sqrt{2}} \\ y_2 = -\frac{d}{\sqrt{2}}, \quad z_2 = -\frac{d}{\sqrt{2}} \\ y_3 = +\frac{d}{\sqrt{2}}, \quad z_3 = -\frac{d}{\sqrt{2}} \\ y_4 = +\frac{d}{\sqrt{2}}, \quad z_4 = +\frac{d}{\sqrt{2}} \end{array} \right.$$

Quindi:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{-ik \frac{d}{\sqrt{2}} \cos \theta} + \right. \\
 & + e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{+ik \frac{d}{\sqrt{2}} \cos \theta} + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{+ik \frac{d}{\sqrt{2}} \cos \theta} + \\
 & \left. + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{-ik \frac{d}{\sqrt{2}} \cos \theta} + 1 \right\} + \\
 & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{-ik \frac{d}{\sqrt{2}} \cos \theta} + \right. \\
 & + e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{+ik \frac{d}{\sqrt{2}} \cos \theta} + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{+ik \frac{d}{\sqrt{2}} \cos \theta} + \\
 & \left. + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{-ik \frac{d}{\sqrt{2}} \cos \theta} + 1 \right\} - \\
 & - \hat{e}_\phi \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{-ik \frac{d}{\sqrt{2}} \cos \theta} + \right. \\
 & + e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{+ik \frac{d}{\sqrt{2}} \cos \theta} + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{+ik \frac{d}{\sqrt{2}} \cos \theta} + \\
 & \left. + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} e^{-ik \frac{d}{\sqrt{2}} \cos \theta} + 1 \right\}
 \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

Si ha:

$$\begin{aligned}
 N_\theta(\theta, \phi) = & \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ e^{+ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} 2 \cos \frac{kd}{\sqrt{2}} \cos \theta + \right. \\
 & \left. + e^{-ik \frac{d}{\sqrt{2}} \sin \theta \sin \phi} 2 \cos \frac{kd}{\sqrt{2}} \cos \theta + 1 \right\} = \\
 = & \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ 4 \left[ \cos \left( \frac{kd}{\sqrt{2}} \sin \theta \sin \phi \right) \right] \left[ \cos \left( \frac{kd}{\sqrt{2}} \cos \theta \right) \right] + 1 \right\}
 \end{aligned}$$

$$N_{\phi}(\theta, \phi) = -\sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left\{ 4 \left[ \cos \left( \frac{kd}{\sqrt{2}} \sin \theta \sin \phi \right) \right] \left[ \cos \left( \frac{kd}{\sqrt{2}} \cos \theta \right) \right] + 1 \right\}$$

$$|N_{\theta}(\theta, \phi)|^2 = \frac{4}{k^2} \cos^2 \theta \cos^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{\left( 1 - \sin^2 \theta \cos^2 \phi \right)^2} \cdot \left\{ 4 \left[ \cos \left( \frac{kd}{\sqrt{2}} \sin \theta \sin \phi \right) \right] \left[ \cos \left( \frac{kd}{\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2$$

$$|N_{\phi}(\theta, \phi)|^2 = \frac{4}{k^2} \sin^2 \phi \frac{\cos^2 \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{\left( 1 - \sin^2 \theta \cos^2 \phi \right)^2} \cdot \left\{ 4 \left[ \cos \left( \frac{kd}{\sqrt{2}} \sin \theta \sin \phi \right) \right] \left[ \cos \left( \frac{kd}{\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2$$

**11-14) Esercizio n. 2 del 1/7/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 90^\circ$ . Si ponga  $d = \frac{3}{4}\lambda$ .

$$|N_\theta(\theta, \phi)|_{(\phi=90^\circ)}^2 = 0$$

$$|N_\phi(\theta, \phi)|_{(\phi=90^\circ)}^2 = \frac{4}{k^2} \left\{ 4 \left[ \cos \left( \frac{kd}{\sqrt{2}} \sin \theta \right) \right] \left[ \cos \left( \frac{kd}{\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2$$

Quindi:

$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=90^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \frac{4}{k^2} \left\{ 4 \left[ \cos \left( \frac{kd}{\sqrt{2}} \sin \theta \right) \right] \left[ \cos \left( \frac{kd}{\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2 \hat{e}_r \end{aligned}$$

Poniamo  $d = \frac{3}{4}\lambda, \implies kd = \frac{3}{2}\pi$ .

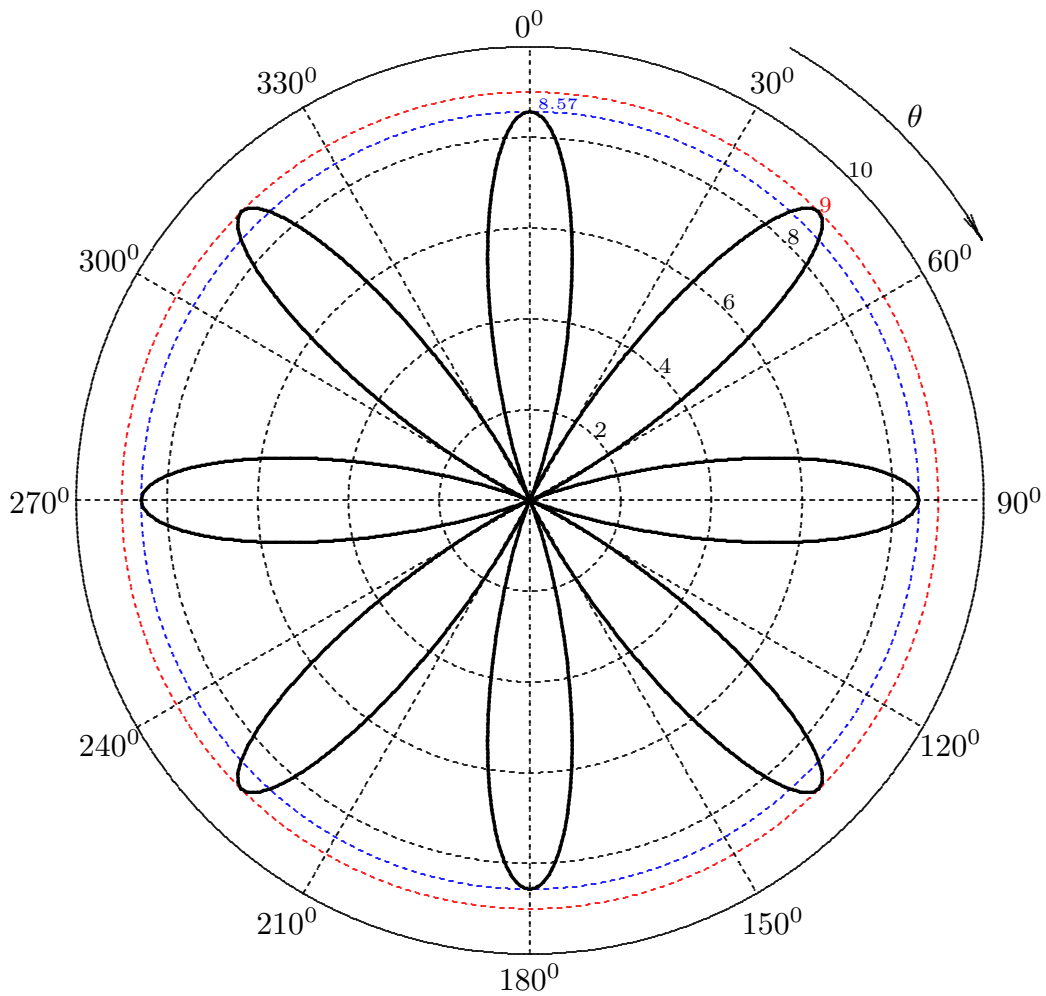
$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=90^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 \left\{ 4 \left[ \cos \left( \frac{3\pi}{2\sqrt{2}} \sin \theta \right) \right] \left[ \cos \left( \frac{3\pi}{2\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2 \hat{e}_r \end{aligned}$$

Grafichiamo il fattore di forma:

$$[F(\theta)]_{(\phi=90^\circ)} = \left\{ 4 \left[ \cos \left( \frac{3\pi}{2\sqrt{2}} \sin \theta \right) \right] \left[ \cos \left( \frac{3\pi}{2\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2$$

**Diagramma di radiazione per  $\phi = 90^\circ$**

$$d = \frac{3}{4}\lambda$$



Poniamo, ora,  $d = \frac{1}{4}\lambda$ ,  $\implies kd = \frac{1}{2}\pi$ .

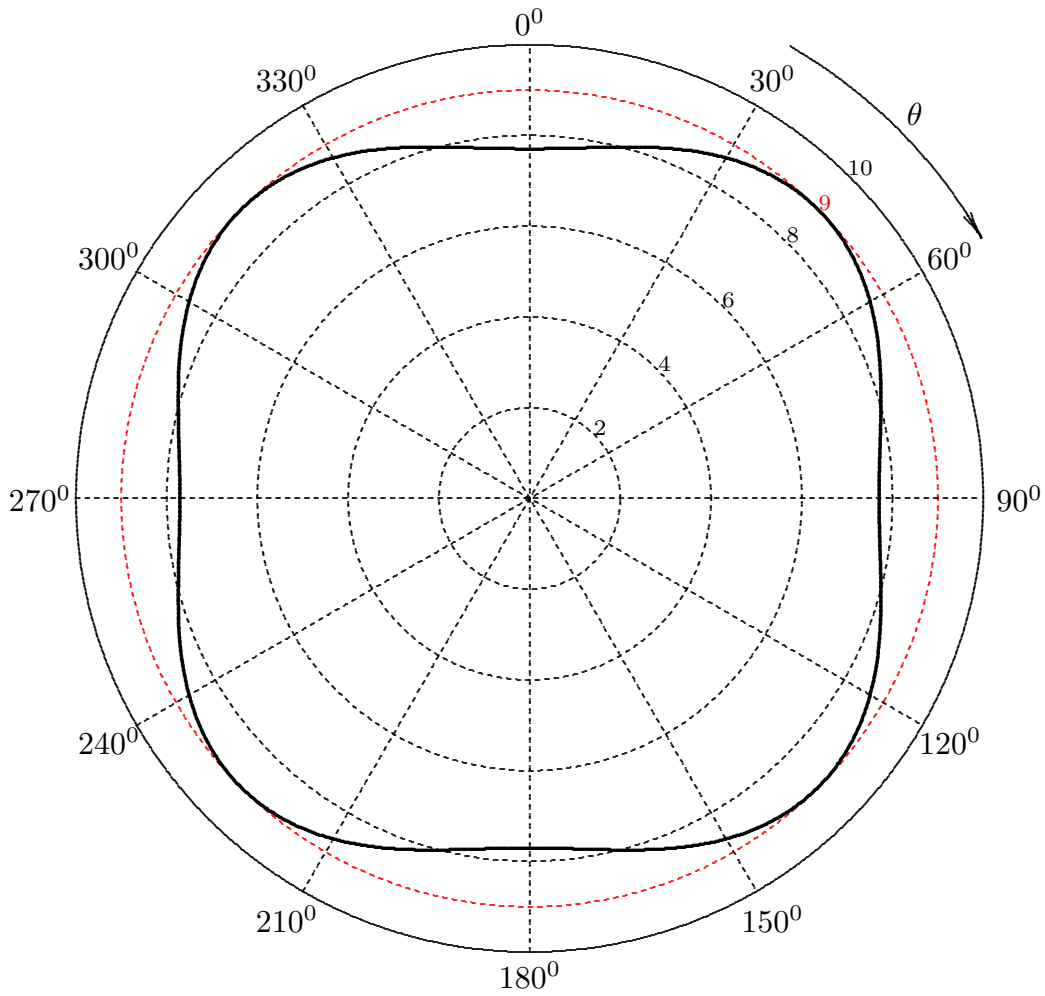
$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=90^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \frac{4}{k^2} \left\{ 4 \left[ \cos \left( \frac{\pi}{2\sqrt{2}} \sin \theta \right) \right] \left[ \cos \left( \frac{\pi}{2\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2 \hat{e}_r \end{aligned}$$

Grafichiamo il fattore di forma:

$$[F(\theta)]_{(\phi=90^\circ)} = \left\{ 4 \left[ \cos \left( \frac{\pi}{2\sqrt{2}} \sin \theta \right) \right] \left[ \cos \left( \frac{\pi}{2\sqrt{2}} \cos \theta \right) \right] + 1 \right\}^2$$

**Diagramma di radiazione per  $\phi = 90^\circ$**

$$d = \frac{1}{4}\lambda$$



**Al diminuire della distanza fra le antenne spariscono i lobi ed il diagramma tende a diventare isotropo nel piano  $\phi = 90^\circ$ .**

**11-15) Esercizio n. 3 del 1/7/2011**

Un fascetto di luce verde ( $\lambda_0 = 514 \text{ nm}$ ) viaggia in un mezzo vetroso (vetro crown) di indice di rifrazione  $n_1 = 1.519$ . Alla fine del mezzo vetroso, sulla sua superficie, vi é depositato un sottilissimo strato di atomi di argento di indice di rifrazione, relativo alla lunghezza d'onda della luce incidente,  $n_r = 0.13$ ,  $n_i = 3.0461$ , di spessore  $d = 15 \text{ nm}$ . Subito dopo c'è l'aria. Calcolare il coefficiente di riflessione.

Il sistema può essere considerato come una lamina piana assorbente (argento) posta fra il vetro ed l'aria.

Dalla teoria delle lamine piane assorbenti si deduce che il coefficiente di riflessione é:

$$R = \frac{|r_{12}|^2 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}^* r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}^* r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12} r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12} r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Cominciamo con il calcolare alcune quantità che servono per la valutazione dei coefficienti che figurano nella formula della riflettività.:

$$(n_1 - n_r) = (1.519 - 0.13) = 1.3890; \quad (n_1 + n_r) = (1.519 + 0.13) = 1.6490$$

$$(n_r - n_3) = (0.13 - 1) = -0.8700; \quad (n_r + n_3) = (0.13 + 1) = 1.13$$

$$[(n_1 - n_r)(n_1 + n_r) - n_i^2] = 1.3890 \cdot 1.6490 - (3.0461)^2 = -6.9883$$

$$[(n_r - n_3)(n_r + n_3) + n_i^2] = -0.8700 \cdot 1.13 + (3.0461)^2 = +8.2956$$

$$[(n_1 + n_r)^2 + n_i^2] = (1.6490)^2 + (3.0461)^2 = 11.9979$$

$$[(n_1 - n_r)^2 + n_i^2] = (1.519)^2 + (3.0461)^2 = 11.2080$$

$$[(n_r + n_3)^2 + n_i^2] = (1.13)^2 + (3.0461)^2 = 10.5556$$

$$[(n_r - n_3)^2 + n_i^2] = (-0.8700)^2 + (3.0461)^2 = 10.0356$$

$$4n_i^2 n_1 n_3 = 4 \cdot (3.0461)^2 \cdot 1.519 = 56.3775$$

$$\begin{aligned} \Re(r_{12}^* r_{23}) &= \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] - 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{(-6.9883)(+8.2956) - 56.3775}{11.9979 \cdot 10.5556} \simeq -\frac{114.3496}{126.6450} \simeq -0.9029 \end{aligned}$$

$$\begin{aligned} \Im(r_{12}^* r_{23}) &= \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] + 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2][(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{2 \cdot 3.0461 \cdot (-6.9883) + 2 \cdot 3.0461 \cdot 1.519 \cdot 8.2956}{126.6450} \simeq \\ &\simeq \frac{-42.5741 + 76.7679}{126.6450} \simeq -\frac{34.1938}{126.6450} \simeq 0.26999 \\ \Re(r_{12} r_{23}) &= \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] + 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2][(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{(-6.9883) \cdot 8.2956 + 56.3775}{126.6450} \simeq -\frac{1.5946}{126.6450} \simeq -0.01259 \\ \Im(r_{12} r_{23}) &= \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] - 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2][(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{-42.5741 - 76.7679}{126.6450} \simeq -\frac{119.3420}{126.6450} \simeq -0.94233 \end{aligned}$$

Inoltre:

$$\begin{aligned} \Re(r_{12}) &= \frac{n_1^2 - n_r^2 - n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{6.9883}{11.9979} \simeq -0.58246 \\ \Re(r_{23}) &= \frac{n_r^2 - n_3^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{8.2956}{10.5556} \simeq +0.78589 \\ \Im(r_{12}) &= \frac{-2n_i n_1}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{9.2541}{11.9976} \simeq -0.7713 \\ \Im(r_{23}) &= \frac{2n_i n_3}{(n_r + n_3)^2 + n_i^2} \simeq \frac{6.0922}{10.5556} \simeq +0.57715 \\ |r_{12}|^2 &= \frac{(n_1 - n_r)^2 + n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq \frac{11.2080}{11.9979} \simeq +0.93416 \\ |r_{23}|^2 &= \frac{(n_r - n_3)^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{10.0356}{10.5556} \simeq +0.950737 \\ \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) &= \sin\left(4\pi \cdot 0.13 \frac{15}{514}\right) \simeq \sin(0.047674) \simeq +0.0476559 \\ \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) &= \cos\left(4\pi \cdot 0.13 \frac{15}{514}\right) \simeq \cos(0.047674) \simeq +0.9988638 \end{aligned}$$

$$\exp\left[-\left(4\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp\left[-\left(4\pi \cdot 3.0461 \frac{15}{514}\right)\right] = \exp(-1.1171) = 0.3272274$$

$$\exp\left[-\left(8\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp\left[-\left(8\pi \cdot 3.0461 \frac{15}{514}\right)\right] = \exp(-2.2342) = 0.1070778$$

Quindi:

$$\begin{aligned} R &= \frac{0.93416 + 0.3272274 \cdot [2 \cdot (-0.9029) \cdot 0.9988638 - 2 \cdot 0.26999 \cdot 0.0476559] + 0.1018028}{1 + 0.3272274[2(-0.01259)(0.9988638) - 2(-0.94233)(0.0476559)] + 0.0951001} \simeq \\ &\simeq \frac{0.4373063}{1.1163} \simeq \underline{\underline{0.391746}} \simeq \underline{\underline{39.17\%}} \end{aligned}$$



**11-16) Esercizio n. 4 del 1/7/2011**

Con riferimento al problema precedente si valuti il coefficiente di trasmissione.

Poiché risulta, in questo caso:

$$\frac{\beta_3 \mu_1}{\beta_1 \mu_3} = \frac{n_3}{n_1}$$

il coefficiente di trasmissione é:

$$T = \frac{\frac{n_3}{n_1} [1 + 2\Re(r_{12}) + |r_{12}|^2] [1 + 2\Re(r_{23}) + |r_{23}|^2] e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)} \right]}$$

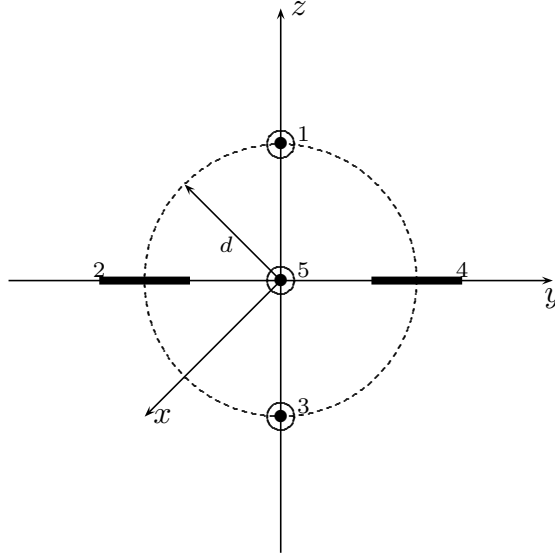
Poiché il coefficiente di trasmissione ha lo stesso denominatore del coefficiente di riflessione, procediamo al calcolo del solo numeratore. Si ha:

$$T = \frac{0.6583278 \cdot [1 + 2 \cdot (-0.58246) + 0.93416] \cdot [1 + 2 \cdot 0.78589 + 0.950737] \cdot 0.3272274}{1.1163} \simeq$$

$$\simeq \frac{0.583723}{1.1163} \simeq \underline{\underline{0.5229087}} \simeq \underline{\underline{52.29\%}}$$

**11-17) Esercizio n. 1 del 29/7/2011**

Sia dato un sistema di 5 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate con i loro centri nel piano  $yz$ . Le correnti sono orientate come in figura. Determinare l'espressione del vettore di Poynting irradiato.



Le densità di corrente sull'antenna 1, sull'antenna 2, sull'antenna 3, sull'antenna 4 e sull'antenna 5 sono rispettivamente:

$$\left\{ \begin{array}{ll} \vec{J}^{(1)} = \hat{x}A_1\delta(y)\delta(z - z_1) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(2)} = \hat{y}A_2\delta(x)\delta(z) \cos k(y - y_2) & y_2 - l \leq y \leq y_2 + l \\ \vec{J}^{(3)} = \hat{x}A_3\delta(y)\delta(z - z_3) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(4)} = \hat{y}A_4\delta(x)\delta(z) \cos k(y - y_4) & y_4 - l \leq y \leq y_4 + l \\ \vec{J}^{(5)} = \hat{x}A_5\delta(y)\delta(z) \cos kx & -l \leq x \leq +l \end{array} \right.$$

Posto  $A_1 = A_2 = A_3 = A_4 = A_5 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante è la somma delle cinque:

$$\vec{J} = \hat{x}\delta(y)\delta(z - z_1) \cos kx + \hat{y}\delta(x)\delta(z) \cos k(y - y_2) + \hat{x}\delta(y)\delta(z - z_3) \cos kx + \hat{y}\delta(x)\delta(z) \cos k(y - y_4) + \hat{x}\delta(y)\delta(z) \cos kx$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  è:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}') d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z' - z_1) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{y} \delta(x') \delta(z') \cos k(y' - y_2) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z' - z_3) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{y} \delta(x') \delta(z') \cos k(y' - y_4) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y') \delta(z') \cos kx' dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{x} e^{-ikz_1 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{y} \int_{y_2-l}^{y_2+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_2) dy' + \\ & + \hat{x} e^{-ikz_3 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{y} \int_{y_4-l}^{y_4+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_4) dy' + \\ & + \hat{x} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' \end{aligned}$$

Si ha:

$$\hat{x} \cdot \hat{r} = \cos \psi = \sin \theta \cos \phi$$

essendo  $\psi$  l'angolo formato fra l'asse  $x$  e la direzione del vettore posizione  $\hat{e}_r$ .

Per un'antenna a mezz'onda, orientata secondo l'asse  $x$ , risulta, quindi:

$$\int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' = \int_{-l}^{+l} e^{-ikx' \cos \psi} \cos kx' dx' = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

Analogamente valutiamo  $\int_{y_i-l}^{y_i+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_i) dy'$ .

Poniamo  $y' - y_i = u \implies dy' = du$ . Per  $y' = y_i - l \implies u = -l$ . Per  $y' = y_i + l \implies u = +l$ . Si ha, quindi:

$$\int_{y_i-l}^{y_i+l} e^{-iky'} \sin \theta \sin \phi \cos k(y' - y_i) dy' =$$

$$= e^{-iky_i \sin \theta \sin \phi} \int_{-l}^{+l} e^{-iku \sin \theta \sin \phi} \cos kudu = e^{-iky_i \sin \theta \sin \phi} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)}$$

avendo calcolato:

$$\int_{-l}^{+l} e^{-iku \sin \theta \sin \phi} \cos kudu = \int_{-l}^{+l} e^{-iku \cos \chi} \cos kudu = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)}$$

in quanto:

$$\hat{y} \cdot \hat{r} = \cos \chi = \sin \theta \sin \phi$$

essendo  $\chi$  l'angolo formato fra l'asse  $y$  e la direzione del vettore posizione  $\hat{e}_r$ .

Ne segue:

$$\vec{N}(\theta, \phi) = \hat{x} e^{-ikz_1} \cos \theta \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} +$$

$$+ \hat{y} e^{-iky_2} \sin \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} +$$

$$+ \hat{x} e^{-ikz_3} \cos \theta \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} +$$

$$+ \hat{y} e^{-iky_4} \sin \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} +$$

$$+ \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

che si può meglio scrivere:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikz_1} \cos \theta + e^{-ikz_3} \cos \theta + 1 \right] +$$

$$+ \hat{y} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{-iky_2} \sin \theta \sin \phi + e^{-iky_4} \sin \theta \sin \phi \right]$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \left\{ \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikz_1 \cos \theta} + e^{-ikz_3 \cos \theta} + 1 \right] + \right. \\
 & \left. + \sin \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_4 \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\theta \left\{ \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikz_1 \cos \theta} + e^{-ikz_3 \cos \theta} + 1 \right] + \right. \\
 & \left. + \cos \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_4 \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\phi \left\{ -\sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikz_1 \cos \theta} + e^{-ikz_3 \cos \theta} + 1 \right] + \right. \\
 & \left. + \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_4 \sin \theta \sin \phi} \right] \right\}
 \end{aligned}$$

Dalla figura risulta:

$$z_1 = +d, \quad z_3 = -d, \quad y_2 = -d, \quad y_4 = +d$$

Quindi:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \left\{ \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + e^{+ikd \cos \theta} + 1 \right] + \right. \\
 & \left. + \sin \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{+ikd \sin \theta \sin \phi} + e^{-ikd \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\theta \left\{ \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + e^{+ikd \cos \theta} + 1 \right] + \right. \\
 & \left. + \cos \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{+ikd \sin \theta \sin \phi} + e^{-ikd \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\phi \left\{ -\sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + e^{+ikd \cos \theta} + 1 \right] + \right. \\
 & \left. + \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ e^{+ikd \sin \theta \sin \phi} + e^{-ikd \sin \theta \sin \phi} \right] \right\}
 \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 (|N_\theta|^2 + |N_\phi|^2) \hat{e}_r$$

Si ha:

$$N_\theta(\theta, \phi) = \left\{ \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} [2 \cos (kd \cos \theta) + 1] + \right. \\ \left. + \cos \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} [2 \cos (kd \sin \theta \sin \phi)] \right\}$$

$$N_\phi(\theta, \phi) = \left\{ -\sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} [2 \cos (kd \cos \theta) + 1] + \right. \\ \left. + \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} [2 \cos (kd \sin \theta \sin \phi)] \right\}$$

**11-18) Esercizio n. 2 del 29/7/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 90^\circ$ . Si ponga  $d = \frac{3}{4}\lambda$ .

$$|N_\theta(\theta, \phi)|_{(\phi=90^\circ)}^2 = \frac{4}{k^2} \left[ \frac{\cos\left(\frac{\pi}{2} \sin \theta\right)}{\cos \theta} [2 \cos(kd \sin \theta)] \right]^2$$

$$|N_\phi(\theta, \phi)|_{(\phi=90^\circ)}^2 = \frac{4}{k^2} \left[ - [2 \cos(kd \cos \theta) + 1] \right]^2$$

Quindi:

$$\langle \vec{S} \rangle_{(\phi=90^\circ)} =$$

$$= \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 \left\{ \left[ \frac{\cos\left(\frac{\pi}{2} \sin \theta\right)}{\cos \theta} [2 \cos(kd \sin \theta)] \right]^2 + \left[ 2 \cos(kd \cos \theta) + 1 \right]^2 \right\} \hat{e}_r$$

Poniamo  $d = \frac{3}{4}\lambda$ ,  $\implies kd = \frac{3}{2}\pi$ .

$$\langle \vec{S} \rangle_{(\phi=90^\circ)} = \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 =$$

$$= \left\{ \left[ \frac{\cos\left(\frac{\pi}{2} \sin \theta\right)}{\cos \theta} \left[ 2 \cos\left(\frac{3}{2}\pi \sin \theta\right) \right] \right]^2 + \left[ 2 \cos\left(\frac{3}{2}\pi \cos \theta\right) + 1 \right]^2 \right\} \hat{e}_r$$

Grafichiamo il fattore di forma:

$$\left\{ \left[ \frac{\cos\left(\frac{\pi}{2} \sin \theta\right)}{\cos \theta} \left[ 2 \cos\left(\frac{3}{2}\pi \sin \theta\right) \right] \right]^2 + \left[ 2 \cos\left(\frac{3}{2}\pi \cos \theta\right) + 1 \right]^2 \right\}$$

Si ha:

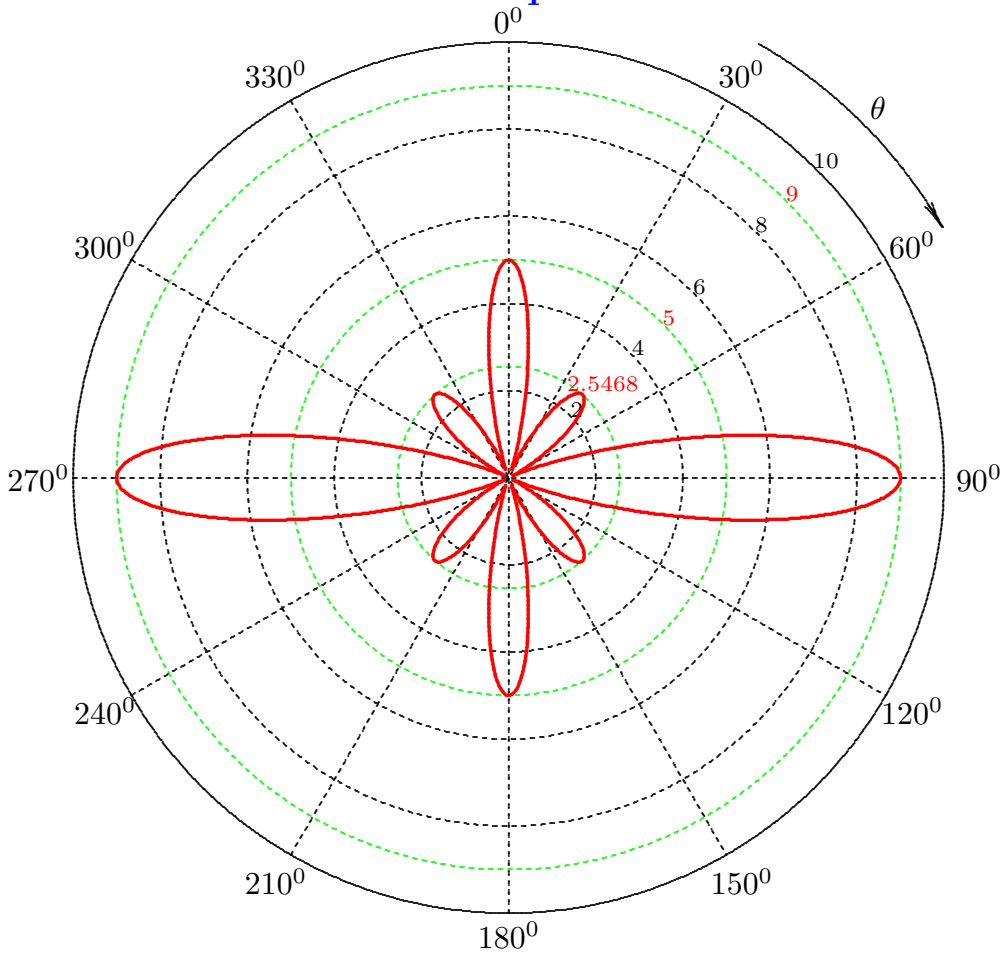
$$\lim_{\theta=90^\circ} \frac{\cos\left(\frac{\pi}{2} \sin \theta\right)}{\cos \theta} = 0$$

Si deduce dalla formula del fattore di forma che esso non si annulla mai, in quanto per annullarsi devono essere contemporaneamente nulli i due termini della somma che non

puó mai avvenire.

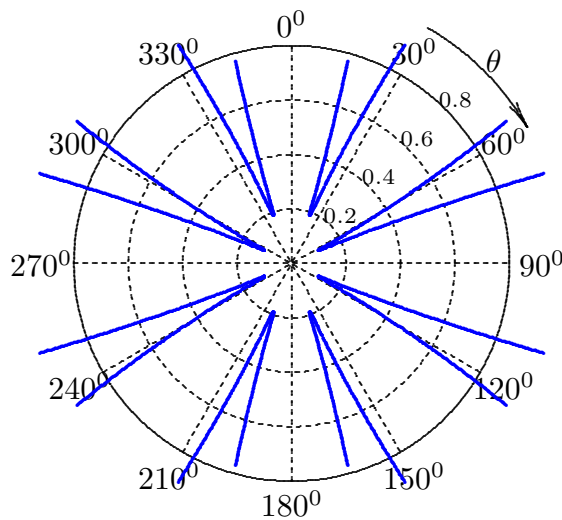
**Diagramma di radiazione per  $\phi = 90^\circ$**

$$d = \frac{3}{4}\lambda$$



Il massimo piú piccolo si trova per  $\theta \simeq 41^\circ.7$  e vale  $\simeq 2.5468$ .

**Ingrandimento del diagramma in prossimitá dello zero**





**11-19) Esercizio n. 3 del 29/7/2011**

Un'onda elettromagnetica piana di frequenza  $\nu = 1 \text{ GHz}$ , viaggiante in aria, incide su una superficie di separazione con un mezzo conduttore i cui parametri costitutivi sono:

$$\epsilon_r = 15, \quad \mu_r \simeq 1, \quad \sigma = 0.84.$$

Graficare il coefficiente di riflessione  $R_{\perp}$  in funzione dell'angolo di incidenza.

(vedi es. n.3 del 29/9/2008 ed es. n.3 del 25/6/2010)

Calcoliamo, relativamente al mezzo conduttore, il rapporto  $\frac{\sigma}{\epsilon\omega}$ :

$$\frac{\sigma}{\epsilon\omega} = \frac{0.84}{8.854 \cdot 10^{-12} \cdot 15 \cdot 2\pi \cdot 10^9} = 1.0066 \implies \left(\frac{\sigma}{\epsilon\omega}\right)^2 = 1.0133$$

da cui:

$$\sqrt{1 + \frac{\sigma^2}{\epsilon^2\omega^2}} = \sqrt{1 + 1.0133} \simeq 1.4189$$

$$\beta_2 = \frac{\omega}{c} \sqrt{\frac{\mu_r\epsilon_r}{2} \left[ 1 + \sqrt{1 + \frac{\sigma^2}{\epsilon^2\omega^2}} \right]} = \frac{\omega}{c} \sqrt{\frac{15}{2} (1 + 1.4189)} \simeq 4.2593 \frac{\omega}{c} \text{ (rad/m)}$$

$$\alpha_2 = \frac{\omega}{c} \sqrt{\frac{\mu_r\epsilon_r}{2} \left[ \sqrt{1 + \frac{\sigma^2}{\epsilon^2\omega^2}} - 1 \right]} = \frac{\omega}{c} \sqrt{\frac{10}{2} (1.4189 - 1)} \simeq 1.7725 \frac{\omega}{c} \text{ (m}^{-1}\text{)}$$

da cui risulta:

$$\beta_2^2 - \alpha_2^2 = \frac{\omega^2}{c^2} \frac{\mu_r\epsilon_r}{2} \left[ 1 + \sqrt{1 + \frac{\sigma^2}{\epsilon^2\omega^2}} \right] - \frac{\omega^2}{c^2} \frac{\mu_r\epsilon_r}{2} \left[ \sqrt{1 + \frac{\sigma^2}{\epsilon^2\omega^2}} - 1 \right] = \frac{\omega^2}{c^2} \mu_r\epsilon_r$$

Si ha anche:

$$\beta_1 = \frac{\omega}{c} \simeq 20.9440 \text{ (rad/m)}$$

$$\begin{aligned} p^2(\theta_0) &= \frac{1}{2} \left[ -\beta_2^2 + \alpha_2^2 + \beta_1^2 \sin^2 \theta_0 + \sqrt{4\beta_2^2\alpha_2^2 + (\beta_2^2 - \alpha_2^2 - \beta_1^2 \sin^2 \theta_0)^2} \right] \simeq \\ &\simeq \frac{1}{2} \frac{\omega^2}{c^2} \left\{ -15 + \sin^2 \theta_0 + \sqrt{227.9864 + (15 - \sin^2 \theta_0)^2} \right\} \end{aligned}$$

$$\begin{aligned} q^2(\theta_0) &= \frac{1}{2} \left[ \beta_2^2 - \alpha_2^2 - \beta_1^2 \sin^2 \theta_0 + \sqrt{4\beta_2^2\alpha_2^2 + (\beta_2^2 - \alpha_2^2 - \beta_1^2 \sin^2 \theta_0)^2} \right] \simeq \\ &\simeq \frac{1}{2} \frac{\omega^2}{c^2} \left\{ 15 - \sin^2 \theta_0 + \sqrt{227.9864 + (15 - \sin^2 \theta_0)^2} \right\} \end{aligned}$$

Il coefficiente di riflessione  $R_{\perp}$ , per  $\mu_1 \simeq \mu_2$ , é:

$$R_{\perp} = \rho_{\perp}^2 = \frac{(q - \beta_1 \cos \theta_0)^2 + p^2}{(q + \beta_1 \cos \theta_0)^2 + p^2}$$

Il coefficiente di riflessione  $R_{\parallel}$ , per  $\mu_1 \simeq \mu_2$ , é:

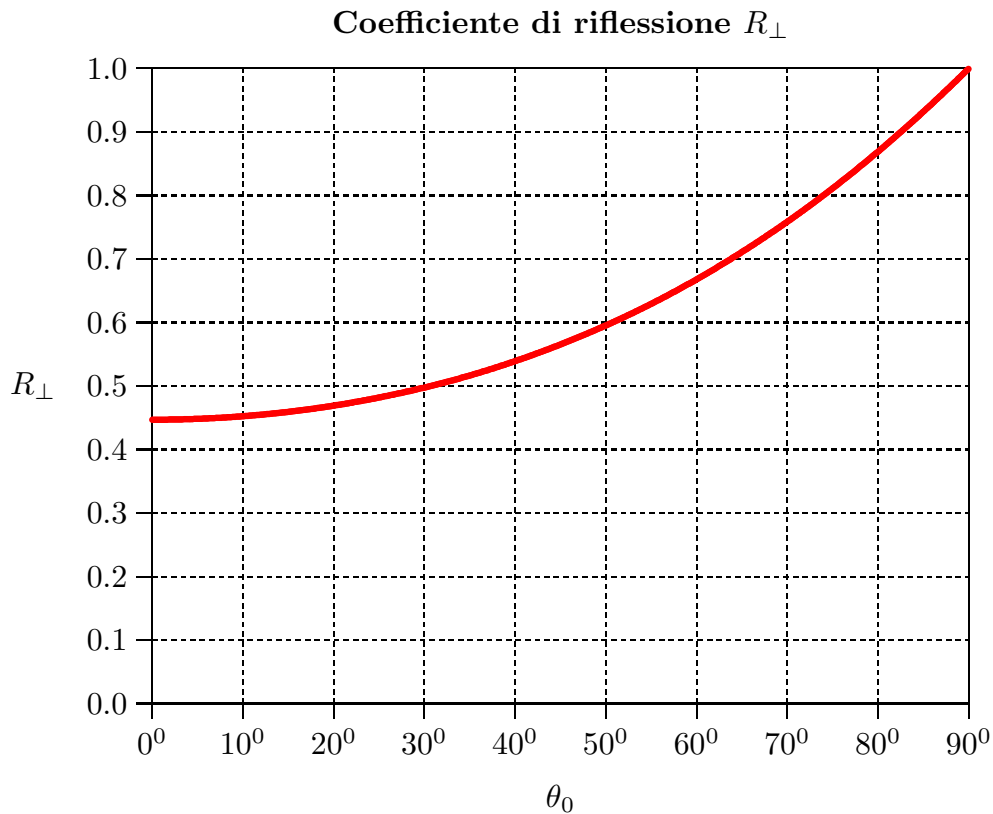
$$R_{\parallel} = \rho_{\parallel}^2 = \rho_{\perp}^2 \frac{(q - \beta_1 \sin \theta_0 \tan \theta_0)^2 + p^2}{(q + \beta_1 \sin \theta_0 \tan \theta_0)^2 + p^2}$$

$\theta_0$	$\frac{p^2 c^2}{\omega^2}$	$\frac{qc}{\omega}$	Num. $R_{\perp}$	Den. $R_{\perp}$	$R_{\perp}$	Num. $R_{\parallel}/\rho_{\perp}^2$	Den. $R_{\parallel}/\rho_{\perp}^2$	$R_{\parallel}$
0°	3.1418	4.2593	13.7650	30.8023	0.4469	21.2836	21.2836	0.4469
5°	3.1429	4.2586	13.7860	30.7554	0.4482	21.2134	21.3433	0.4455
10°	3.1463	4.2563	13.8489	30.6155	0.4524	21.0027	21.5240	0.4414
15°	3.1517	4.2526	13.9540	30.3849	0.4592	20.6514	21.8311	0.4344
20°	3.1592	4.2476	14.1015	30.0672	0.4690	20.1593	22.2744	0.4245
25°	3.1684	4.2414	14.2914	29.6676	0.4817	19.5252	22.8687	0.4113
30°	3.1791	4.2343	14.5242	29.1921	0.4975	18.7468	23.6362	0.3946
35°	3.1910	4.2263	14.8000	29.1921	0.5166	17.8195	24.6091	0.3741
40°	3.2038	4.2179	15.1191	28.0435	0.5391	16.7354	25.8353	0.3492
45°	3.2171	4.2092	15.4816	27.3869	0.5653	15.4816	27.3869	0.3196
50°	3.2305	4.2004	15.8874	26.6873	0.5953	14.0382	29.3771	0.2845
55°	3.2463	4.1920	16.3363	25.9540	0.6294	12.3766	31.9929	0.2435
60°	3.2559	4.1840	16.8278	25.1959	0.6679	10.4598	35.5639	0.1964
65°	3.2672	4.1768	17.3611	24.4219	0.7109	8.2545	40.7264	0.1441
70°	3.2769	4.1706	17.9349	23.6406	0.7586	5.8012	48.8716	0.0900
71°	3.2786	4.1695	18.0544	23.4842	0.7688	5.3050	51.1024	0.0798
72°	3.2803	4.1684	18.1754	23.3278	0.7791	4.8213	53.6261	0.0700
73°	3.2819	4.1674	18.2979	23.1716	0.7897	4.3624	56.5040	0.0610
74°	3.2834	4.1665	18.4219	23.0156	0.8004	3.9462	59.8154	0.0528
75°	3.2848	4.1656	18.5474	22.8599	0.8114	3.5992	63.6645	0.0459
76°	3.2862	4.1647	18.6744	22.7045	0.8225	3.3607	68.1908	0.0405
77°	3.2875	4.1639	18.8028	22.5495	0.8338	3.2907	73.5849	0.0373
77° .1	3.2876	4.1638	18.8157	22.5340	0.8350	3.2961	74.1815	0.0371
77° .2	3.2877	4.1637	18.8286	22.5185	0.8361	3.3042	74.7896	0.03694
77° .3	3.2878	4.1637	18.8416	22.5030	0.8373	3.3151	75.4097	0.03681
77° .4	3.2879	4.1636	18.8545	22.4876	0.8384	3.3289	76.0419	0.03670
77° .5	3.2881	4.1635	18.8675	22.4721	0.8396	3.3458	76.6868	0.03663
77° .6	3.2882	4.1634	18.8805	22.4566	0.8407	3.3658	77.3446	0.036588
77° .7	3.2883	4.1634	18.8935	22.4412	0.8419	3.3893	78.0158	0.036575
77° .8	3.2884	4.1633	18.9065	22.4257	0.8431	3.4162	78.7007	0.036595

77 <sup>0.9</sup>	3.2885	4.1632	18.9195	22.4103	0.8442	3.4467	79.3998	0.03665
78 <sup>0</sup>	3.2886	4.1632	18.9326	22.3948	0.8454	3.4811	80.1135	0.03673
79 <sup>0</sup>	3.2897	4.1625	19.0638	22.2407	0.8572	4.0775	88.1599	0.03964
80 <sup>0</sup>	3.2907	4.1618	19.1963	22.0871	0.8691	5.3165	98.2939	0.0470
81 <sup>0</sup>	3.2916	4.1613	19.3303	21.9341	0.8813	7.5962	111.395	0.0601
82 <sup>0</sup>	3.2924	4.1607	19.4655	21.7817	0.8937	11.6178	128.886	0.0806
83 <sup>0</sup>	3.2932	4.1603	19.6020	21.6300	0.9062	18.6858	153.207	0.1105
84 <sup>0</sup>	3.2938	4.1599	19.7398	21.4791	0.9190	31.4087	188.856	0.1528
85 <sup>0</sup>	3.2943	4.1596	19.8788	21.3289	0.9320	55.5239	244.976	0.2112
86 <sup>0</sup>	3.2948	4.1593	20.0190	21.1795	0.9452	105.437	342.779	0.2907
87 <sup>0</sup>	3.2951	4.1591	20.1603	21.0310	0.9586	225.183	542.187	0.3981
88 <sup>0</sup>	3.2953	4.1589	20.3028	20.8834	0.9722	601.582	1077.7	0.5427
89 <sup>0</sup>	3.2955	4.1588	20.4464	20.7367	0.9860	2825.3	3778.2	0.7373
90 <sup>0</sup>	3.2955	4.1588	20.5911	20.5911	1	∞	∞	1

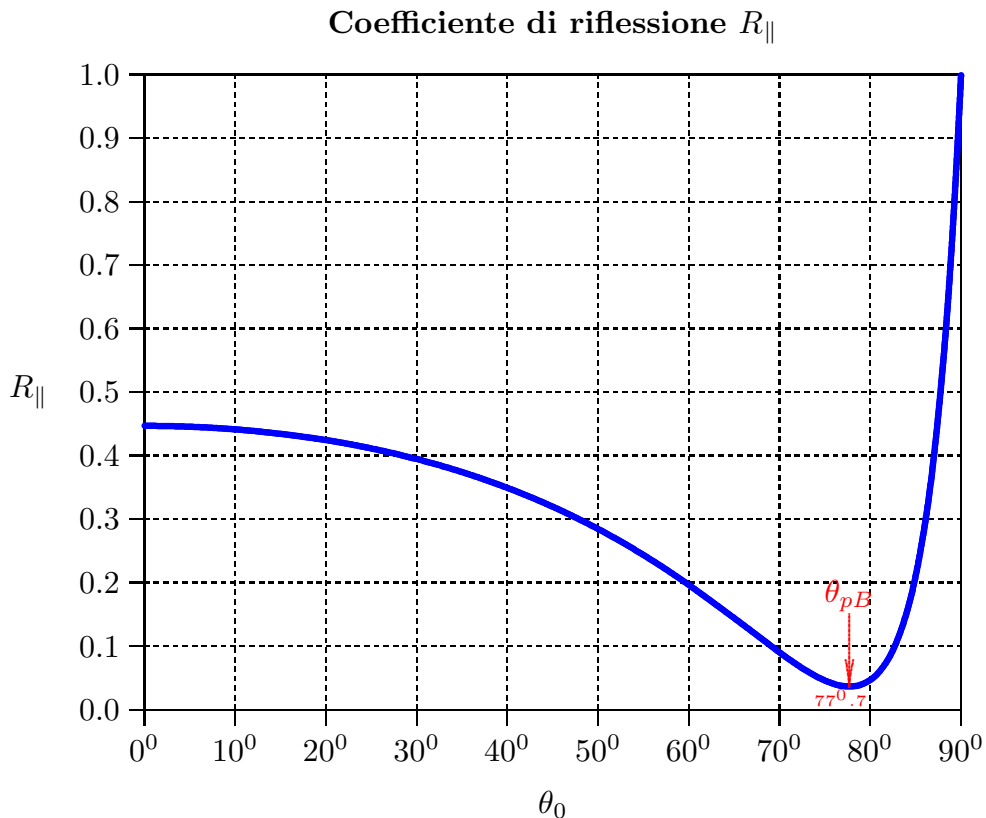
Per  $\theta_0 = 90^0$   $R_{\parallel}$  é una forma indeterminata  $\frac{\infty}{\infty}$  che determinata (dividendo numeratore e denominatore per  $\tan \theta_0$ ) risulta 1.

I numeratori ed i denominatori di  $R_{\perp}$  e  $R_{\parallel}$  indicati in tabella sono calcolati a meno di  $\frac{\omega}{c}$ .



**11-20) Esercizio n. 4 del 29/7/2011**

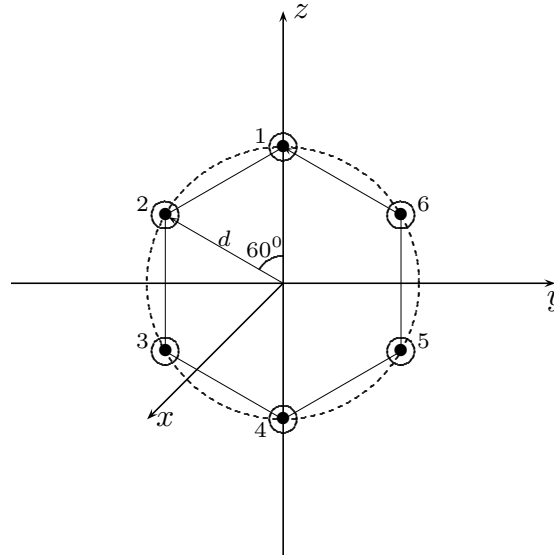
Con riferimento al problema precedente si grafichi il coefficiente di riflessione  $R_{\parallel}$  in funzione dell'angolo di incidenza. Si valuti l'angolo pseudoBrewster ed il valore del coefficiente di riflessione ad esso corrispondente.



Dalla tabella dell'esercizio precedente e dal grafico di  $R_{\parallel}$  si deduce che l'angolo pseudoBrewster  $\theta_{pB}$  vale  $77^{\circ}.7$  ed il valore minimo del coefficiente di riflessione, in corrispondenza di tale angolo, é  $\simeq 3.6\%$ .

**11-21) Esercizio n. 1 del 16/9/2011**

Sia dato un sistema di 6 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate con i loro centri nel piano  $yz$  ai vertici di un esagono regolare inscritto in una circonferenza di raggio  $d$ . Le correnti sono orientate lungo l'asse  $x$ , come in figura. Determinare l'espressione del vettore di Poynting irradiato.



Le densità di corrente sull'antenna 1, sull'antenna 2, sull'antenna 3, sull'antenna 4, sull'antenna 5 e sull'antenna 6 sono rispettivamente:

$$\left\{ \begin{array}{ll} \vec{J}^{(1)} = \hat{x}A_1\delta(y - y_1)\delta(z - z_1) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(2)} = \hat{x}A_2\delta(y - y_2)\delta(z - z_2) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(3)} = \hat{x}A_3\delta(y - y_3)\delta(z - z_3) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(4)} = \hat{x}A_4\delta(y - y_4)\delta(z - z_4) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(5)} = \hat{x}A_5\delta(y - y_5)\delta(z - z_5) \cos kx & -l \leq x \leq +l \\ \vec{J}^{(6)} = \hat{x}A_6\delta(y - y_6)\delta(z - z_6) \cos kx & -l \leq x \leq +l \end{array} \right.$$

Posto  $A_1 = A_2 = A_3 = A_4 = A_5 = A_6 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante é la somma delle sei:

$$\vec{J} = \hat{x}\delta(y - y_1)\delta(z - z_1) \cos kx + \hat{x}\delta(y - y_2)\delta(z - z_2) \cos kx + \hat{x}\delta(y - y_3)\delta(z - z_3) \cos kx + \hat{x}\delta(y - y_4)\delta(z - z_4) \cos kx + \hat{x}\delta(y - y_5)\delta(z - z_5) \cos kx + \hat{x}\delta(y - y_6)\delta(z - z_6) \cos kx$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  é:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}') d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_1) \delta(z' - z_1) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_2) \delta(z' - z_2) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_3) \delta(z' - z_3) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_4) \delta(z' - z_4) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_5) \delta(z' - z_5) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_6) \delta(z' - z_6) \cos kx' dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{x} e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_5 \sin \theta \sin \phi} e^{-ikz_5 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_6 \sin \theta \sin \phi} e^{-ikz_6 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' \end{aligned}$$

Si ha:

$$\hat{x} \cdot \hat{r} = \cos \psi = \sin \theta \cos \phi$$

essendo  $\psi$  l'angolo formato fra l'asse  $x$  e la direzione del vettore posizione  $\hat{e}_r$ .

Per un'antenna a mezz'onda, orientata secondo l'asse  $x$ , risulta, quindi:

$$\int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' = \int_{-l}^{+l} e^{-ikx' \cos \psi} \cos kx' dx' = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

Ne segue:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} + \right. \\ \left. + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} + \right. \\ \left. + e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} + e^{-iky_5 \sin \theta \sin \phi} e^{-ikz_5 \cos \theta} + \right. \\ \left. + e^{-iky_6 \sin \theta \sin \phi} e^{-ikz_6 \cos \theta} \right]$$

Si ha:

$$\left\{ \begin{array}{ll} y_1 = 0; & z_1 = +d \\ y_2 = -d \cos 30^\circ; & z_2 = +d \sin 30^\circ \\ y_3 = -d \cos 30^\circ; & z_3 = -d \sin 30^\circ \\ y_4 = 0; & z_4 = -d \\ y_5 = +d \cos 30^\circ; & z_5 = -d \sin 30^\circ \\ y_6 = +d \cos 30^\circ; & z_6 = +d \sin 30^\circ \end{array} \right.$$

Quindi:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ \frac{e^{-ikd \cos \theta}}{e} + \frac{e^{+ik \frac{\sqrt{3}d}{2} \sin \theta \sin \phi} e^{-ik \frac{d}{2} \cos \theta}}{e} + \right. \\ \left. + \frac{e^{+ik \frac{\sqrt{3}d}{2} \sin \theta \sin \phi} e^{+ik \frac{d}{2} \cos \theta}}{e} + \frac{e^{+ikd \cos \theta}}{e} + \frac{e^{-ik \frac{\sqrt{3}d}{2} \sin \theta \sin \phi} e^{+ik \frac{d}{2} \cos \theta}}{e} + \right. \\ \left. + \frac{e^{-ik \frac{\sqrt{3}d}{2} \sin \theta \sin \phi} e^{-ik \frac{d}{2} \cos \theta}}{e} \right]$$

Accoppiando i termini sottolineati si ha:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + e^{+ik \frac{\sqrt{3}d}{2} \sin \theta \sin \phi} \cos\left(k \frac{d}{2} \cos \theta\right) + e^{-ik \frac{\sqrt{3}d}{2} \sin \theta \sin \phi} \cos\left(k \frac{d}{2} \cos \theta\right) \right]$$

ossia:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta \sin \phi\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right]$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned} \vec{N}(\theta, \phi) &= \\ &= \hat{e}_r \sin \theta \cos \phi \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta \sin \phi\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right] + \\ &+ \hat{e}_\theta \cos \theta \cos \phi \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta \sin \phi\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right] + \\ &+ \hat{e}_\phi (-\sin \phi) \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta \sin \phi\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right] \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

essendo:

$$N_\theta(\theta, \phi) = \cos \theta \cos \phi \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta \sin \phi\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right]$$

$$N_\phi(\theta, \phi) = (-\sin \phi) \frac{4 \cos\left(\frac{\pi}{2} \sin \theta \cos \phi\right)}{k \left(1 - \sin^2 \theta \cos^2 \phi\right)} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta \sin \phi\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right]$$



**11-22) Esercizio n. 2 del 16/9/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 90^\circ$  ( $yz$ ). Si ponga  $d = \lambda$ .

$$|N_\theta(\theta, \phi)|_{(\phi=90^\circ)}^2 = 0$$

$$|N_\phi(\theta, \phi)|_{(\phi=90^\circ)}^2 = \frac{16}{k^2} \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right]^2$$

Quindi:

$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=90^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{1}{\pi r} \right)^2 \left[ \cos(kd \cos \theta) + 2 \cos\left(k \frac{\sqrt{3}d}{2} \sin \theta\right) \cos\left(k \frac{d}{2} \cos \theta\right) \right]^2 \hat{e}_r \end{aligned}$$

Poniamo  $d = \lambda$ ,  $\implies kd = 2\pi$ .

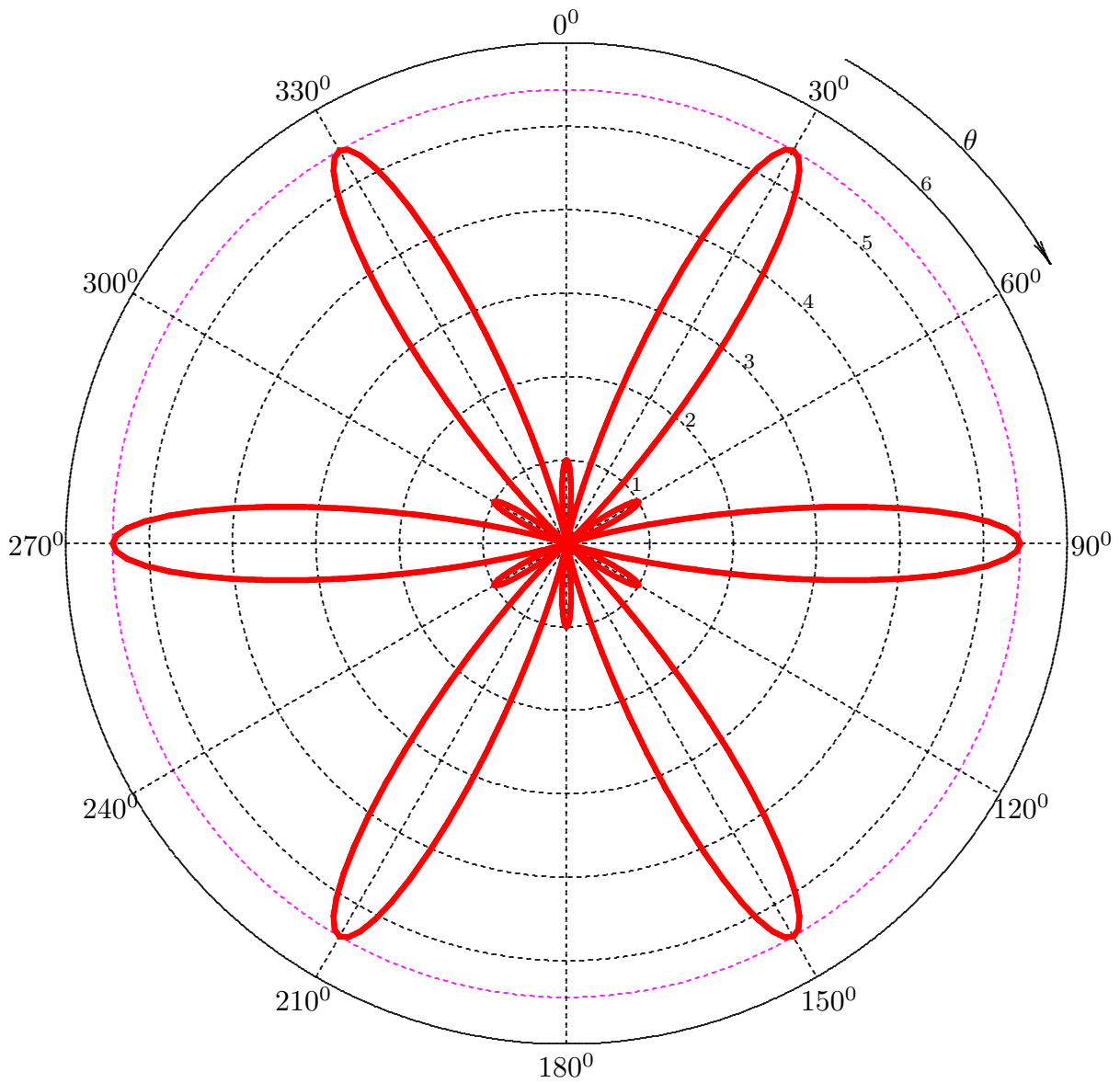
$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=90^\circ)} &= \\ &= \frac{1}{2} Z \left( \frac{1}{\pi r} \right)^2 \left[ \cos(2\pi \cos \theta) + 2 \cos\left(\sqrt{3}\pi \sin \theta\right) \cos(\pi \cos \theta) \right]^2 \hat{e}_r \end{aligned}$$

Grafichiamo il fattore di forma:

$$F(\theta) = \left[ \cos(2\pi \cos \theta) + 2 \cos\left(\sqrt{3}\pi \sin \theta\right) \cos(\pi \cos \theta) \right]^2$$

**Diagramma di radiazione per  $\phi = 90^\circ$**

$d = \lambda$

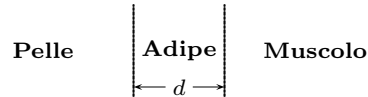


Il valore massimo dei lobi grandi vale  $\simeq 5.4394$ .

**11-23) Esercizio n. 3 del 16/9/2011**

Un'onda elettromagnetica piana di frequenza  $\nu = 1.5 \text{ GHz}$ , viaggiante in aria, incide sulla pelle di un corpo umano nella direzione della normale alla superficie. Sotto la pelle c'è un tessuto adiposo e al di sotto ancora un tessuto muscolare.

La pelle ed i muscoli sono tessuti con alto contenuto d'acqua e pertanto hanno una elevata permittività dielettrica. Per semplificazione ne trascuriamo la conducibilità che, del resto, non è molto alta. Si consideri allora un sistema costituito dai tre mezzi pelle-adipe-muscolo.



I parametri costitutivi di tali mezzi, relativi alla frequenza data, sono:

- Pelle :  $\epsilon_{r1} \simeq 49$ ,  $\sigma_1 \simeq 0$  (con approssimazione),  $\mu \simeq \mu_0$
- Adipe :  $\epsilon_{r2} \simeq 5.6$ ,  $\sigma_2 \simeq 100 \text{ S/m}$ ,  $\mu \simeq \mu_0$
- Muscolo :  $\epsilon_{r3} \simeq 49$ ,  $\sigma_3 \simeq 0$  (con approssimazione),  $\mu \simeq \mu_0$

Calcolare il coefficiente di riflessione dal tessuto adiposo se lo spessore di esso è  $d = 1 \text{ mm}$ .

Scriviamo le formule che legano gli indici di rifrazione ai parametri costitutivi dei tre mezzi, attraverso le costanti di propagazione  $\beta$  ed i coefficienti di attenuazione  $\alpha$  dell'onda elettromagnetica:

$$\beta_1 = \frac{\omega}{c} n_1, \quad \beta_2 = \frac{\omega}{c} \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ 1 + \sqrt{1 + \frac{\sigma_2^2}{\epsilon_2^2 \omega^2}} \right]} = \frac{\omega}{c} n_r,$$

$$\alpha_2 = \frac{\omega}{c} \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ \sqrt{1 + \frac{\sigma_2^2}{\epsilon_2^2 \omega^2}} - 1 \right]} = \frac{\omega}{c} n_i, \quad \beta_3 = \frac{\omega}{c} n_3$$

Per il primo mezzo, risulta  $n_1 = \sqrt{\epsilon_{r1}} = \sqrt{49} = 7$ . Per il secondo mezzo, si ha:

$$n_r = \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ 1 + \sqrt{1 + \frac{\sigma_2^2}{\epsilon_2^2 \omega^2}} \right]}, \quad n_i = \sqrt{\frac{\mu_{r2} \epsilon_{r2}}{2} \left[ \sqrt{1 + \frac{\sigma_2^2}{\epsilon_2^2 \omega^2}} - 1 \right]}$$

Si ha:

$$\frac{\sigma_2^2}{\epsilon_2^2 \omega^2} = \frac{10^4}{(8.854 \cdot 10^{-12} \cdot 5.6 \cdot 2\pi \cdot 1.5 \cdot 10^9)^2} \simeq 4.5793 \cdot 10^4 \gg 1$$

ossia:

$$\left[ 1 + \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} \right] \simeq \left[ \sqrt{1 + \frac{\sigma^2}{\epsilon_2^2 \omega^2}} - 1 \right] \simeq \sqrt{\frac{\sigma^2}{\epsilon_2^2 \omega^2}} \simeq 213.9939$$

per cui si può approssimare:

$$n_r \simeq n_i \simeq \sqrt{\frac{5.6}{2}} 213.9939 \simeq 24.4782$$

Il sistema può essere considerato come una lamina piana assorbente (adipe) posta fra la pelle ed il muscolo.

Dalla teoria delle lamine piane assorbenti si deduce che il coefficiente di riflessione é:

$$R = \frac{|r_{12}|^2 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}^* r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}^* r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12} r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12} r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Cominciamo con il calcolare alcune quantità che servono per la valutazione dei coefficienti che figurano nella formula della riflettività.:

$$(n_1 - n_r) = (7 - 24.4782) = -17.4782; \quad (n_1 + n_r) = (7 + 24.4782) = 31.4782$$

$$(n_r - n_3) = (24.4782 - 7) = +17.4782; \quad (n_r + n_3) = (24.4782 + 7) = 31.4782$$

$$[(n_1 - n_r)(n_1 + n_r) - n_i^2] = -17.4782 \cdot 31.4782 - (24.4782)^2 = -1.1494 \cdot 10^3$$

$$[(n_r - n_3)(n_r + n_3) + n_i^2] = 17.4782 \cdot 31.4782 + (24.4782)^2 = +1.1494 \cdot 10^3$$

$$[(n_1 + n_r)^2 + n_i^2] = (7 + 24.4782)^2 + (24.4782)^2 = 1.5901 \cdot 10^3$$

$$[(n_1 - n_r)^2 + n_i^2] = (7 - 24.4782)^2 + (24.4782)^2 = 904.6698$$

$$[(n_r + n_3)^2 + n_i^2] = (24.4782 + 7)^2 + (24.4782)^2 = 1.5901 \cdot 10^3$$

$$[(n_r - n_3)^2 + n_i^2] = (24.4782 - 7)^2 + (24.4782)^2 = 904.6698$$

$$4n_i^2 n_1 n_3 = 4(24.4782)^2 \cdot 7 \cdot 7 = 1.1744 \cdot 10^5$$

$$\begin{aligned} \Re(r_{12}^* r_{23}) &= \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] - 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{(-1.1494 \cdot 10^3)(+1.1494 \cdot 10^3) - 1.1744 \cdot 10^5}{(1.5901 \cdot 10^3)^2} \simeq -\frac{1.4386 \cdot 10^6}{2.5284 \cdot 10^6} \simeq -0.5690 \end{aligned}$$

$$\begin{aligned} \Im(r_{12}^* r_{23}) &= \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] + 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq \\ &\simeq \frac{2 \cdot 24.4782 \cdot 7 \cdot (-1.1494 \cdot 10^3) + 2 \cdot 24.4782 \cdot 7 \cdot (+1.1494 \cdot 10^3)}{2.5284 \cdot 10^6} = 0 \end{aligned}$$

$$\Re(r_{12}r_{23}) = \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] + 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq$$

$$\simeq \frac{(-1.1494 \cdot 10^3)(+1.1494 \cdot 10^3) + 1.1744 \cdot 10^5}{2.5284 \cdot 10^6} \simeq -\frac{1.2037 \cdot 10^6}{2.5284 \cdot 10^6} \simeq -0.4761$$

$$\Im(r_{12}r_{23}) = \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] - 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq$$

$$\simeq \frac{2 \cdot 24.4782 \cdot 7 \cdot (-1.1494 \cdot 10^3) - 2 \cdot 24.4782 \cdot 7 \cdot (+1.1494 \cdot 10^3)}{2.5284 \cdot 10^6} \simeq$$

$$\simeq \frac{-3.9389 \cdot 10^5 - 3.9389 \cdot 10^5}{2.5284 \cdot 10^6} \simeq -\frac{7.8779 \cdot 10^5}{2.5284 \cdot 10^6} \simeq -0.3116$$

Inoltre:

$$\Re(r_{12}) = \frac{n_1^2 - n_r^2 - n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{1.1494 \cdot 10^3}{1.5901 \cdot 10^3} \simeq -0.7228$$

$$\Re(r_{23}) = \frac{n_r^2 - n_3^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq +\frac{1.1494 \cdot 10^3}{1.5901 \cdot 10^3} \simeq +0.7228$$

$$\Im(r_{12}) = \frac{-2n_i n_1}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{342.6948}{1.5901 \cdot 10^3} \simeq -0.2155$$

$$\Im(r_{23}) = \frac{2n_i n_3}{(n_r + n_3)^2 + n_i^2} \simeq +\frac{342.6948}{1.5901 \cdot 10^3} \simeq +0.2155$$

$$|r_{12}|^2 = \frac{(n_1 - n_r)^2 + n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq +\frac{904.6698}{1.5901 \cdot 10^3} \simeq +0.5689$$

$$|r_{23}|^2 = \frac{(n_r - n_3)^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq +\frac{904.6698}{1.5901 \cdot 10^3} \simeq +0.5689$$

$$\lambda_0 = \frac{c}{\nu} = \frac{3 \cdot 10^8}{1.5 \cdot 10^9} = 0.2 \text{ m} = 20 \text{ cm} \quad \frac{d}{\lambda_0} = \frac{10^{-3}}{0.2} = 0.005$$

$$\sin\left(4\pi n_r \frac{d}{\lambda_0}\right) = \sin(4\pi \cdot 24.4782 \cdot 0.005) \simeq +0.9995$$

$$\cos\left(4\pi n_r \frac{d}{\lambda_0}\right) = \cos(4\pi \cdot 24.4782 \cdot 0.005) \simeq +0.0328$$

$$\exp\left[-\left(4\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp[-(4\pi \cdot 24.4782 \cdot 0.005)] = +0.2148$$

$$\exp\left[-\left(8\pi n_i \frac{d}{\lambda_0}\right)\right] = \exp[-(8\pi \cdot 24.4782 \cdot 0.005)] = +0.0461$$

Quindi:

$$R = \frac{0.5689 + 0.2148 [2(-0.5690)0.0328] + 0.5689 \cdot 0.0461}{1 + 0.2148[2(-0.4761)(0.0328) - 2(-0.3116)(0.9995)] + 0.0149} \simeq$$

$$\simeq \frac{0.5871}{1.1420} \simeq \underline{\underline{0.5141}} \simeq \underline{\underline{51.41\%}}$$

**11-24) Esercizio n. 4 del 16/9/2011**

Con riferimento al problema precedente si valuti il coefficiente di trasmissione.

Poiché risulta, in questo caso:

$$\frac{\beta_3 \mu_1}{\beta_1 \mu_3} = \frac{n_3}{n_1}$$

il coefficiente di trasmissione é:

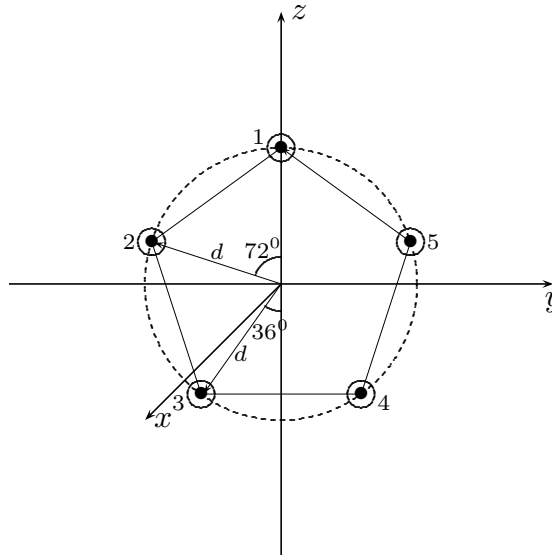
$$T = \frac{\frac{n_3}{n_1} [1 + 2\Re(r_{12}) + |r_{12}|^2] [1 + 2\Re(r_{23}) + |r_{23}|^2] e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Poiché il coefficiente di trasmissione ha lo stesso denominatore del coefficiente di riflessione, procediamo al calcolo del solo numeratore. Si ha:

$$T = \frac{[1 - 2 \cdot 0.7228 + 0.5689] [1 + 2 \cdot 0.7228 + 0.5689] 0.2148}{1.1420} \simeq \frac{0.0798}{1.1420} \simeq \underline{\underline{\simeq 0.0699 \simeq 6.99\%}}$$

**11-25) Esercizio n. 1 del 7/10/2011**

Sia dato un sistema di 5 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate con i loro centri nel piano  $yz$  ai vertici di un pentagono regolare inscritto in una circonferenza di raggio  $d$ . Le correnti sono orientate lungo l'asse  $x$ , come in figura. Determinare l'espressione del vettore di Poynting irradiato.



Le densità di corrente sull'antenna 1, sull'antenna 2, sull'antenna 3, sull'antenna 4 e sull'antenna 5 sono rispettivamente:

$$\left\{ \begin{array}{l} \vec{J}^{(1)} = \hat{x}A_1\delta(y - y_1)\delta(z - z_1) \cos kx \quad -l \leq x \leq +l \\ \vec{J}^{(2)} = \hat{x}A_2\delta(y - y_2)\delta(z - z_2) \cos kx \quad -l \leq x \leq +l \\ \vec{J}^{(3)} = \hat{x}A_3\delta(y - y_3)\delta(z - z_3) \cos kx \quad -l \leq x \leq +l \\ \vec{J}^{(4)} = \hat{x}A_4\delta(y - y_4)\delta(z - z_4) \cos kx \quad -l \leq x \leq +l \\ \vec{J}^{(5)} = \hat{x}A_5\delta(y - y_5)\delta(z - z_5) \cos kx \quad -l \leq x \leq +l \end{array} \right.$$

Posto  $A_1 = A_2 = A_3 = A_4 = A_5 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante é la somma delle sei:

$$\vec{J} = \hat{x}\delta(y - y_1)\delta(z - z_1) \cos kx + \hat{x}\delta(y - y_2)\delta(z - z_2) \cos kx + \hat{x}\delta(y - y_3)\delta(z - z_3) \cos kx + \hat{x}\delta(y - y_4)\delta(z - z_4) \cos kx + \hat{x}\delta(y - y_5)\delta(z - z_5) \cos kx$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  é:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}') d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_1) \delta(z' - z_1) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_2) \delta(z' - z_2) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_3) \delta(z' - z_3) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_4) \delta(z' - z_4) \cos kx' dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{x} \delta(y' - y_5) \delta(z' - z_5) \cos kx' dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{x} e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' + \\ & + \hat{x} e^{-iky_5 \sin \theta \sin \phi} e^{-ikz_5 \cos \theta} \int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' \end{aligned}$$

Si ha:

$$\hat{x} \cdot \hat{r} = \cos \psi = \sin \theta \cos \phi$$

essendo  $\psi$  l'angolo formato fra l'asse  $x$  e la direzione del vettore posizione  $\hat{e}_r$ .



Per un'antenna a mezz'onda, orientata secondo l'asse  $x$ , risulta, quindi:

$$\int_{-l}^{+l} e^{-ikx' \sin \theta \cos \phi} \cos kx' dx' = \int_{-l}^{+l} e^{-ikx' \cos \psi} \cos kx' dx' = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)}$$

Ne segue:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-iky_1 \sin \theta \sin \phi} e^{-ikz_1 \cos \theta} + \right. \\ \left. + e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} + \right. \\ \left. + e^{-iky_4 \sin \theta \sin \phi} e^{-ikz_4 \cos \theta} + e^{-iky_5 \sin \theta \sin \phi} e^{-ikz_5 \cos \theta} \right]$$

Si ha:

$$\left\{ \begin{array}{ll} y_1 = 0; & z_1 = +d \\ y_2 = -d \cos 18^\circ; & z_2 = +d \sin 18^\circ \\ y_3 = -d \sin 36^\circ; & z_3 = -d \cos 36^\circ \\ y_4 = +d \sin 36^\circ; & z_4 = -d \cos 36^\circ \\ y_5 = +d \cos 18^\circ; & z_5 = +d \sin 18^\circ \end{array} \right.$$

Quindi:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ \left. + \underline{e^{+ikd \cos 18^\circ \sin \theta \sin \phi} e^{-ikd \sin 18^\circ \cos \theta}} + \underline{e^{+ikd \sin 36^\circ \sin \theta \sin \phi} e^{+ikd \cos 36^\circ \cos \theta}} + \right. \\ \left. + \underline{e^{-ikd \sin 36^\circ \sin \theta \sin \phi} e^{+ikd \cos 36^\circ \cos \theta}} + \underline{e^{-ikd \cos 18^\circ \sin \theta \sin \phi} e^{-ikd \sin 18^\circ \cos \theta}} \right]$$

Accoppiando i termini sottolineati si ha:

$$\vec{N}(\theta, \phi) = \hat{x} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ \left. + 2e^{-ikd \sin 18^\circ \cos \theta} \cos (kd \cos 18^\circ \sin \theta \sin \phi) + \right. \\ \left. + 2e^{+ikd \cos 36^\circ \cos \theta} \cos (kd \sin 36^\circ \sin \theta \sin \phi) \right]$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{e}_r \sin \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ & + 2e^{-ikd \sin 18^\circ \cos \theta} \cos (kd \cos 18^\circ \sin \theta \sin \phi) + \\ & \left. + 2e^{+ikd \cos 36^\circ \cos \theta} \cos (kd \sin 36^\circ \sin \theta \sin \phi) \right] + \\ & + \hat{e}_\theta \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ & + 2e^{-ikd \sin 18^\circ \cos \theta} \cos (kd \cos 18^\circ \sin \theta \sin \phi) + \\ & \left. + 2e^{+ikd \cos 36^\circ \cos \theta} \cos (kd \sin 36^\circ \sin \theta \sin \phi) \right] + \\ & + \hat{e}_\phi (-\sin \phi) \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ & + 2e^{-ikd \sin 18^\circ \cos \theta} \cos (kd \cos 18^\circ \sin \theta \sin \phi) + \\ & \left. + 2e^{+ikd \cos 36^\circ \cos \theta} \cos (kd \sin 36^\circ \sin \theta \sin \phi) \right] \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

essendo:

$$\begin{aligned} N_\theta(\theta, \phi) = & \cos \theta \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ & + 2e^{-ikd \sin 18^\circ \cos \theta} \cos (kd \cos 18^\circ \sin \theta \sin \phi) + \\ & \left. + 2e^{+ikd \cos 36^\circ \cos \theta} \cos (kd \sin 36^\circ \sin \theta \sin \phi) \right] \end{aligned}$$

$$N_{\phi}(\theta, \phi) = (-\sin \phi) \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \left[ e^{-ikd \cos \theta} + \right. \\ \left. + 2e^{-ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 2e^{+ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) \right]$$

Per valutare il modulo quadro delle componenti  $N_{\theta}$  e  $N_{\phi}$ , moltiplichiamo l'espressione all'interno delle parentesi quadre per la complessa coniugata; si ha:

$$\left[ e^{-ikd \cos \theta} + 2e^{-ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 2e^{+ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) \right] \cdot \\ \cdot \left[ e^{+ikd \cos \theta} + 2e^{+ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 2e^{-ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) \right] = \\ = \left[ 1 + 2e^{-ikd \cos \theta} e^{+ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 2e^{-ikd \cos \theta} e^{-ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 2e^{+ikd \cos \theta} e^{-ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 4 [\cos (kd \cos 18^{\circ} \sin \theta \sin \phi)]^2 + \right. \\ \left. + 4e^{-ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) \cdot \right. \\ \left. \cdot e^{-ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 2e^{+ikd \cos \theta} e^{+ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 4e^{+ikd \cos 36^{\circ} \cos \theta} \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) \cdot \right. \\ \left. \cdot e^{+ikd \sin 18^{\circ} \cos \theta} \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\ \left. + 4 [\cos (kd \sin 36^{\circ} \sin \theta \sin \phi)]^2 \right]$$

che si può scrivere:

$$\begin{aligned}
 & \left[ e^{-ikd \cos \theta} + 2e^{-ikd \sin 18^\circ \cos \theta} \cos(kd \cos 18^\circ \sin \theta \sin \phi) + \right. \\
 & \left. + 2e^{+ikd \cos 36^\circ \cos \theta} \cos(kd \sin 36^\circ \sin \theta \sin \phi) \right] \cdot \\
 & \cdot \left[ e^{+ikd \cos \theta} + 2e^{+ikd \sin 18^\circ \cos \theta} \cos(kd \cos 18^\circ \sin \theta \sin \phi) + \right. \\
 & \left. + 2e^{-ikd \cos 36^\circ \cos \theta} \cos(kd \sin 36^\circ \sin \theta \sin \phi) \right] = \\
 & = \left[ 1 + \underline{2e^{-ikd \cos \theta(1 - \sin 18^\circ)} \cos(kd \cos 18^\circ \sin \theta \sin \phi)} + \right. \\
 & \left. + \underline{\underline{2e^{-ikd \cos \theta(1 + \cos 36^\circ)} \cos(kd \sin 36^\circ \sin \theta \sin \phi)}} + \right. \\
 & \left. + \underline{\underline{2e^{+ikd \cos \theta(1 - \sin 18^\circ)} \cos(kd \cos 18^\circ \sin \theta \sin \phi)}} + \right. \\
 & + 4 [\cos(kd \cos 18^\circ \sin \theta \sin \phi)]^2 + \\
 & \left. + \underline{\underline{\underline{4e^{-ikd \cos \theta(\sin 18^\circ + \cos 36^\circ)} \cos(kd \cos 18^\circ \sin \theta \sin \phi) \cos(kd \sin 36^\circ \sin \theta \sin \phi)}}}} + \right. \\
 & \left. + \underline{\underline{\underline{2e^{+ikd \cos \theta(1 + \cos 36^\circ)} \cos(kd \sin 36^\circ \sin \theta \sin \phi)}}}} + \right. \\
 & \left. + \underline{\underline{\underline{4e^{+ikd \cos \theta(\cos 36^\circ + \sin 18^\circ)} \cos(kd \sin 36^\circ \sin \theta \sin \phi) \cos(kd \cos 18^\circ \sin \theta \sin \phi)}}}} + \right. \\
 & \left. + 4 [\cos(kd \sin 36^\circ \sin \theta \sin \phi)]^2 \right] = \\
 & = \left[ 1 + 4 \cos[kd \cos \theta(1 - \sin 18^\circ)] \cos(kd \cos 18^\circ \sin \theta \sin \phi) + \right. \\
 & + 4 \cos[kd \cos \theta(1 + \cos 36^\circ)] \cos(kd \sin 36^\circ \sin \theta \sin \phi) + \\
 & + 4 [\cos(kd \cos 18^\circ \sin \theta \sin \phi)]^2 + \\
 & + 8 \cos(kd \cos 18^\circ \sin \theta \sin \phi) \cos(kd \sin 36^\circ \sin \theta \sin \phi) \cos[kd \cos \theta(\sin 18^\circ + \cos 36^\circ)] + \\
 & \left. + 4 [\cos(kd \sin 36^\circ \sin \theta \sin \phi)]^2 \right]
 \end{aligned}$$

Pertanto:

$$\begin{aligned}
 |N_{\theta}(\theta, \phi)|^2 &= \cos^2 \theta \cos^2 \phi \left[ \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \right]^2 \cdot \\
 &\cdot \left[ 1 + 4 \cos [kd \cos \theta (1 - \sin 18^{\circ})] \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\
 &+ 4 \cos [kd \cos \theta (1 + \cos 36^{\circ})] \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \\
 &+ 4 [\cos (kd \cos 18^{\circ} \sin \theta \sin \phi)]^2 + \\
 &+ 8 \cos [kd \cos \theta (\sin 18^{\circ} + \cos 36^{\circ})] \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \\
 &\left. + 4 [\cos (kd \sin 36^{\circ} \sin \theta \sin \phi)]^2 \right] \\
 |N_{\phi}(\theta, \phi)|^2 &= \sin^2 \phi \left[ \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \cos \phi \right)}{k \left( 1 - \sin^2 \theta \cos^2 \phi \right)} \right]^2 \cdot \\
 &\cdot \left[ 1 + 4 \cos [kd \cos \theta (1 - \sin 18^{\circ})] \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) + \right. \\
 &+ 4 \cos [kd \cos \theta (1 + \cos 36^{\circ})] \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \\
 &+ 4 [\cos (kd \cos 18^{\circ} \sin \theta \sin \phi)]^2 + \\
 &+ 8 \cos [kd \cos \theta (\sin 18^{\circ} + \cos 36^{\circ})] \cos (kd \cos 18^{\circ} \sin \theta \sin \phi) \cos (kd \sin 36^{\circ} \sin \theta \sin \phi) + \\
 &\left. + 4 [\cos (kd \sin 36^{\circ} \sin \theta \sin \phi)]^2 \right]
 \end{aligned}$$

**11-26) Esercizio n. 2 del 7/10/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 90^\circ$  ( $yz$ ). Si ponga  $d = \lambda$ .

$$|N_\theta(\theta, \phi)|_{(\phi=90^\circ)}^2 = 0$$

$$|N_\phi(\theta, \phi)|_{(\phi=90^\circ)}^2 = \frac{4}{k^2} \left\{ 1 + 4 \cos [kd \cos \theta (1 - \sin 18^\circ)] \cos (kd \cos 18^\circ \sin \theta) + \right. \\ \left. + 4 \cos [kd \cos \theta (1 + \cos 36^\circ)] \cos (kd \sin 36^\circ \sin \theta) + 4 [\cos (kd \cos 18^\circ \sin \theta)]^2 + \right. \\ \left. + 8 \cos [kd \cos \theta (\sin 18^\circ + \cos 36^\circ)] \cos (kd \cos 18^\circ \sin \theta) \cos (kd \sin 36^\circ \sin \theta) + \right. \\ \left. + 4 [\cos (kd \sin 36^\circ \sin \theta)]^2 \right\}$$

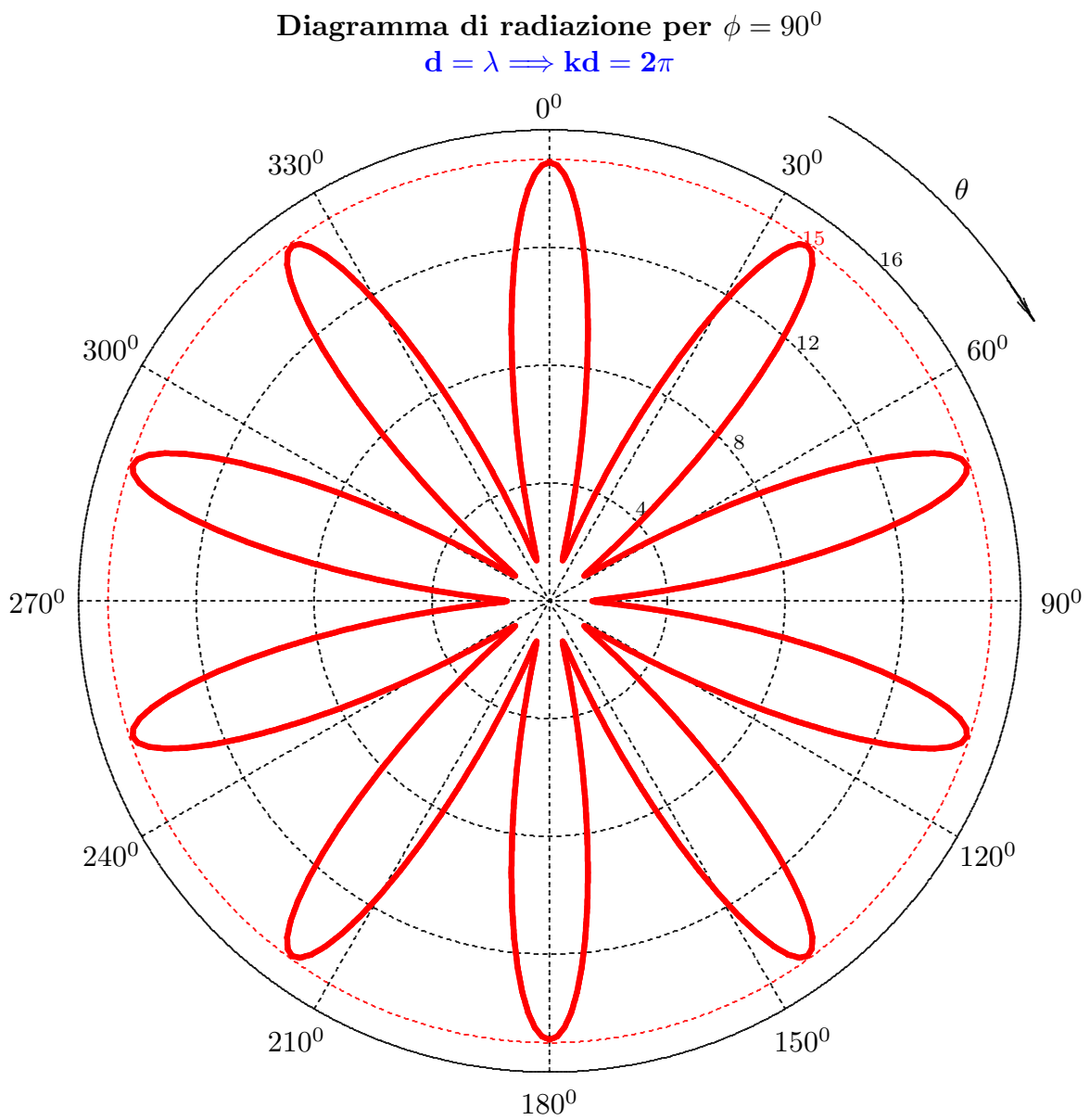
Quindi:

$$\langle \vec{S} \rangle_{(\phi=90^\circ)} = \\ = \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 \left\{ 1 + 4 \cos [kd \cos \theta (1 - \sin 18^\circ)] \cos (kd \cos 18^\circ \sin \theta) + \right. \\ \left. + 4 \cos [kd \cos \theta (1 + \cos 36^\circ)] \cos (kd \sin 36^\circ \sin \theta) + 4 [\cos (kd \cos 18^\circ \sin \theta)]^2 + \right. \\ \left. + 8 \cos [kd \cos \theta (\sin 18^\circ + \cos 36^\circ)] \cos (kd \cos 18^\circ \sin \theta) \cos (kd \sin 36^\circ \sin \theta) + \right. \\ \left. + 4 [\cos (kd \sin 36^\circ \sin \theta)]^2 \right\} \hat{e}_r$$

Il fattore di forma che esprime il diagramma di radiazione nel piano  $\phi = 90^\circ$  é, quindi:

$$F(\theta) = \left\{ 1 + 4 \cos [kd \cos \theta (1 - \sin 18^\circ)] \cos (kd \cos 18^\circ \sin \theta) + \right. \\ \left. + 4 \cos [kd \cos \theta (1 + \cos 36^\circ)] \cos (kd \sin 36^\circ \sin \theta) + 4 [\cos (kd \cos 18^\circ \sin \theta)]^2 + \right. \\ \left. + 8 \cos [kd \cos \theta (\sin 18^\circ + \cos 36^\circ)] \cos (kd \cos 18^\circ \sin \theta) \cos (kd \sin 36^\circ \sin \theta) + \right. \\ \left. + 4 [\cos (kd \sin 36^\circ \sin \theta)]^2 \right\}$$

Grafichiamo il fattore di forma per  $d = \lambda \implies kd = 2\pi$ .



Grafichiamo il fattore di forma per altri valori di  $d$ .

Diagramma di radiazione per  $\phi = 90^\circ$

$$d = \frac{3}{4}\lambda \implies kd = \frac{3}{2}\pi$$

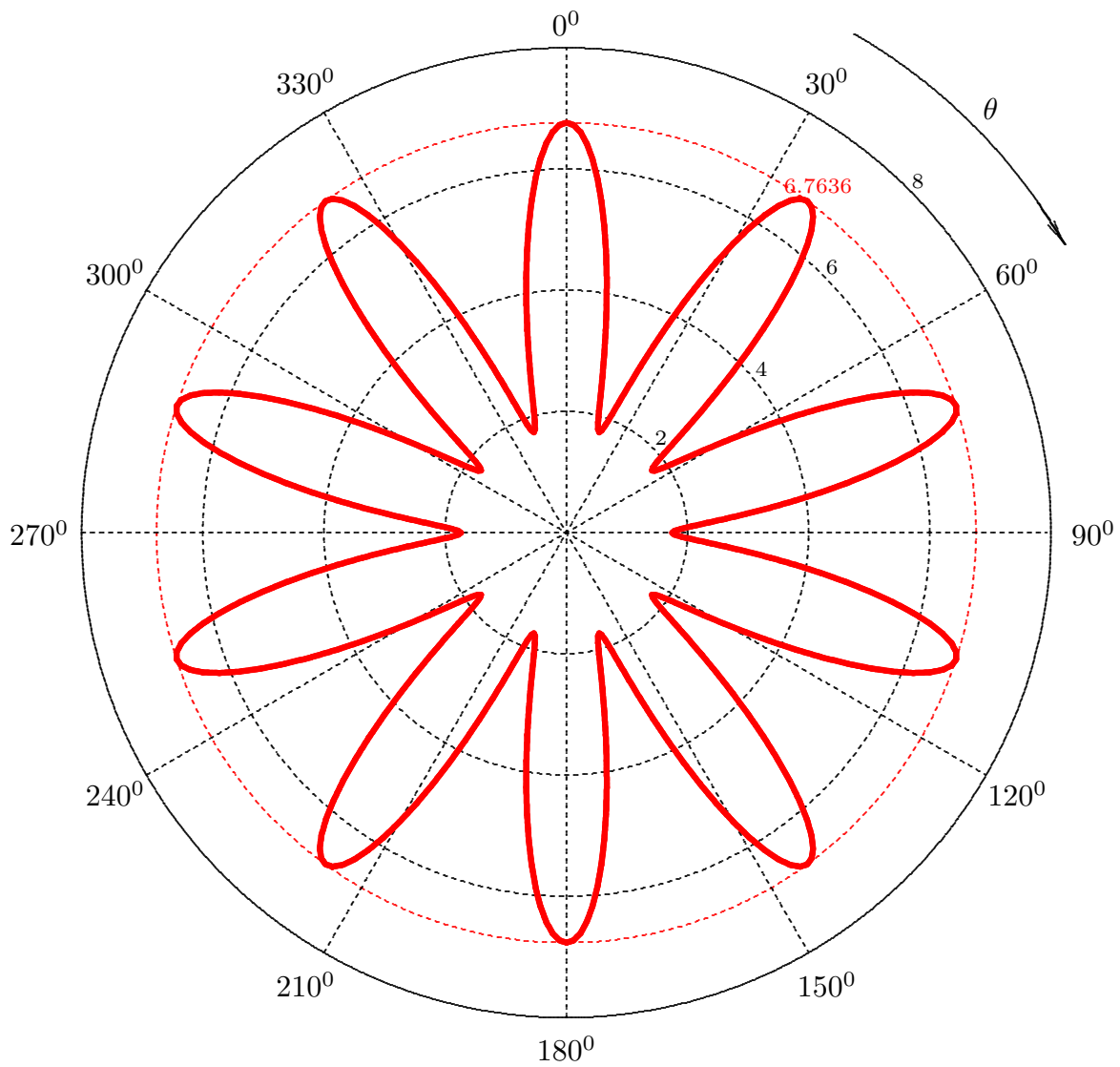
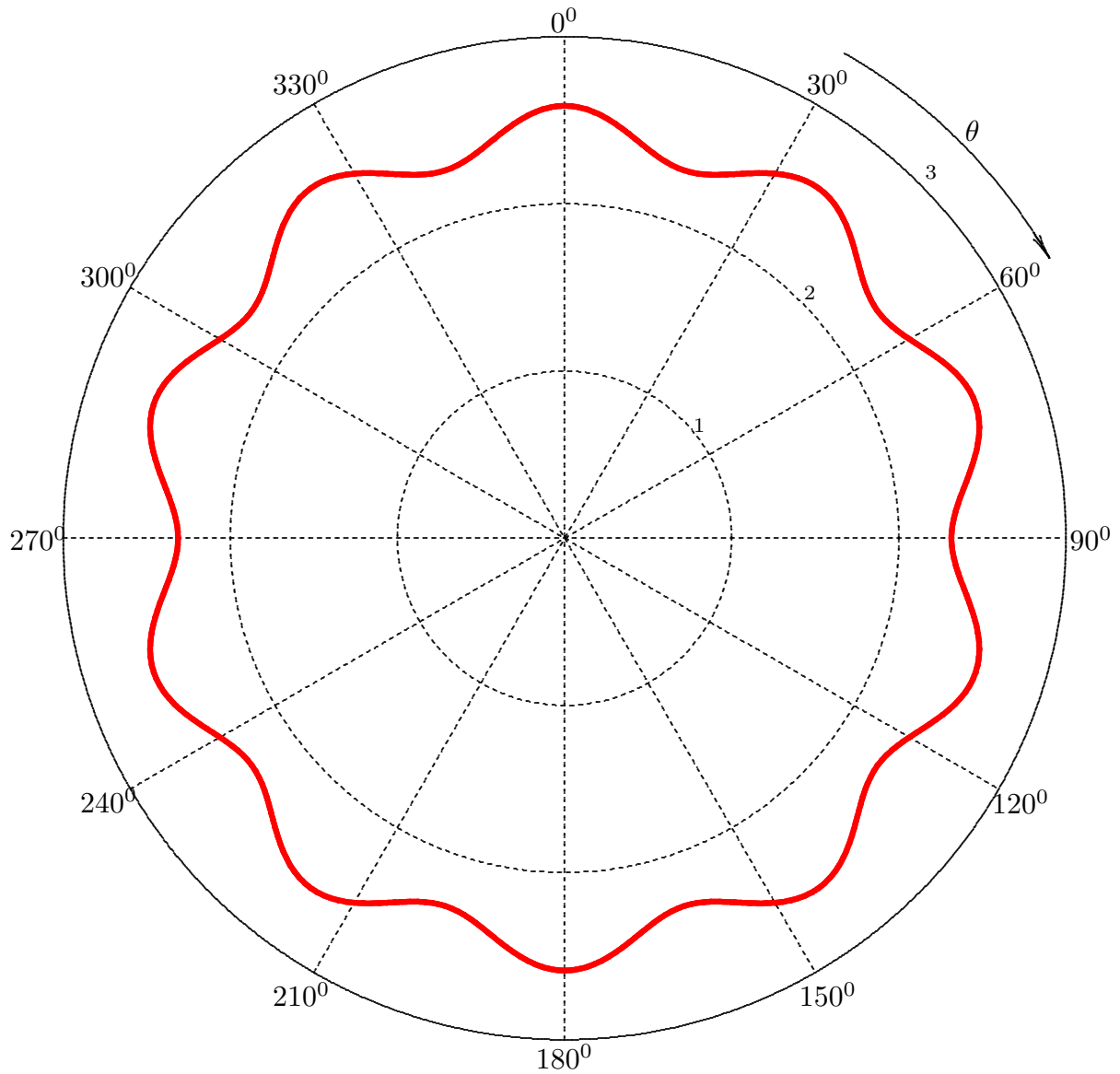




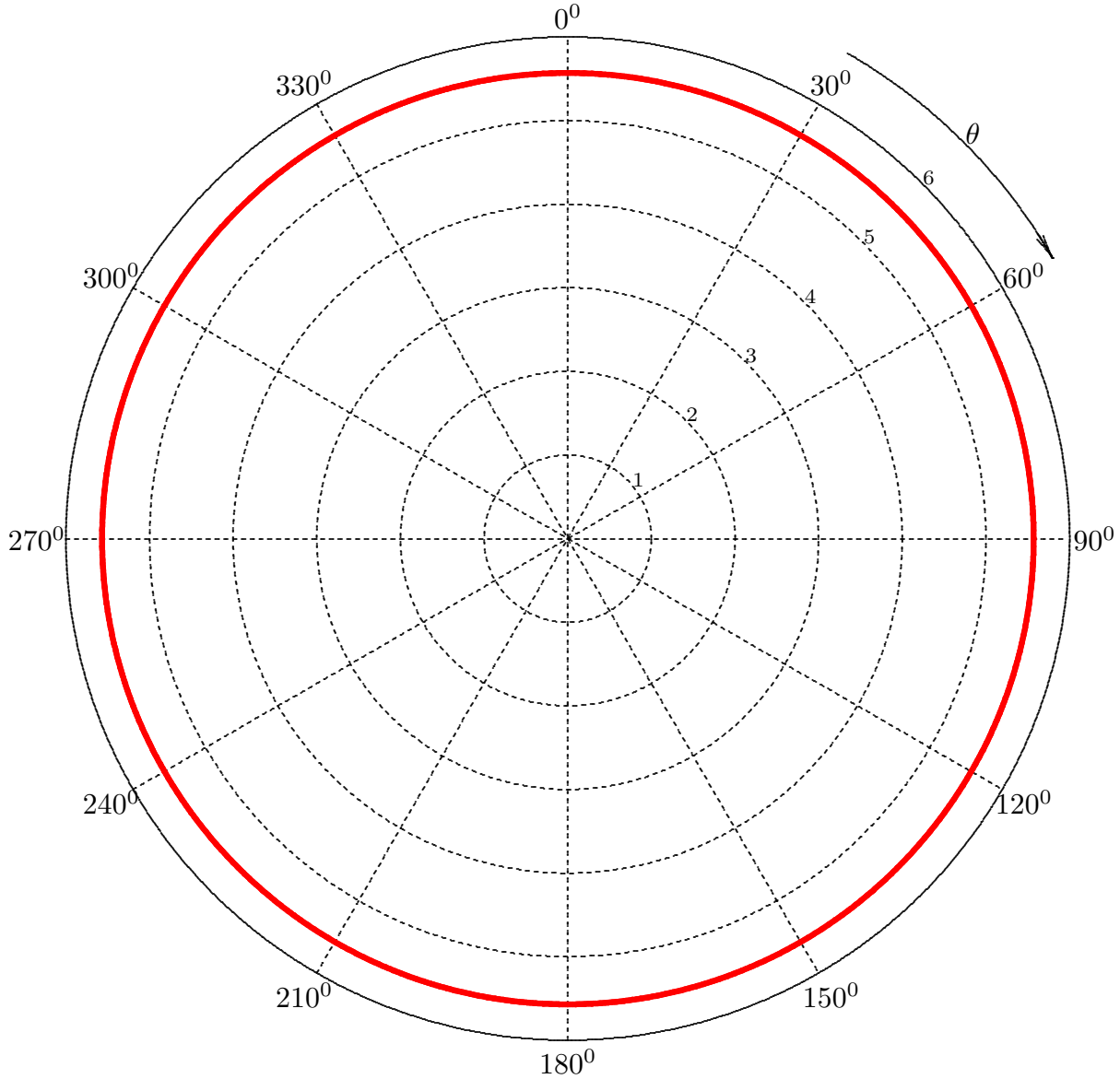
Diagramma di radiazione per  $\phi = 90^\circ$

$$d = \frac{\lambda}{2} \implies kd = \pi$$



**Diagramma di radiazione per  $\phi = 90^\circ$**

$$\mathbf{d = \frac{\lambda}{4} \implies kd = \frac{\pi}{2}}$$



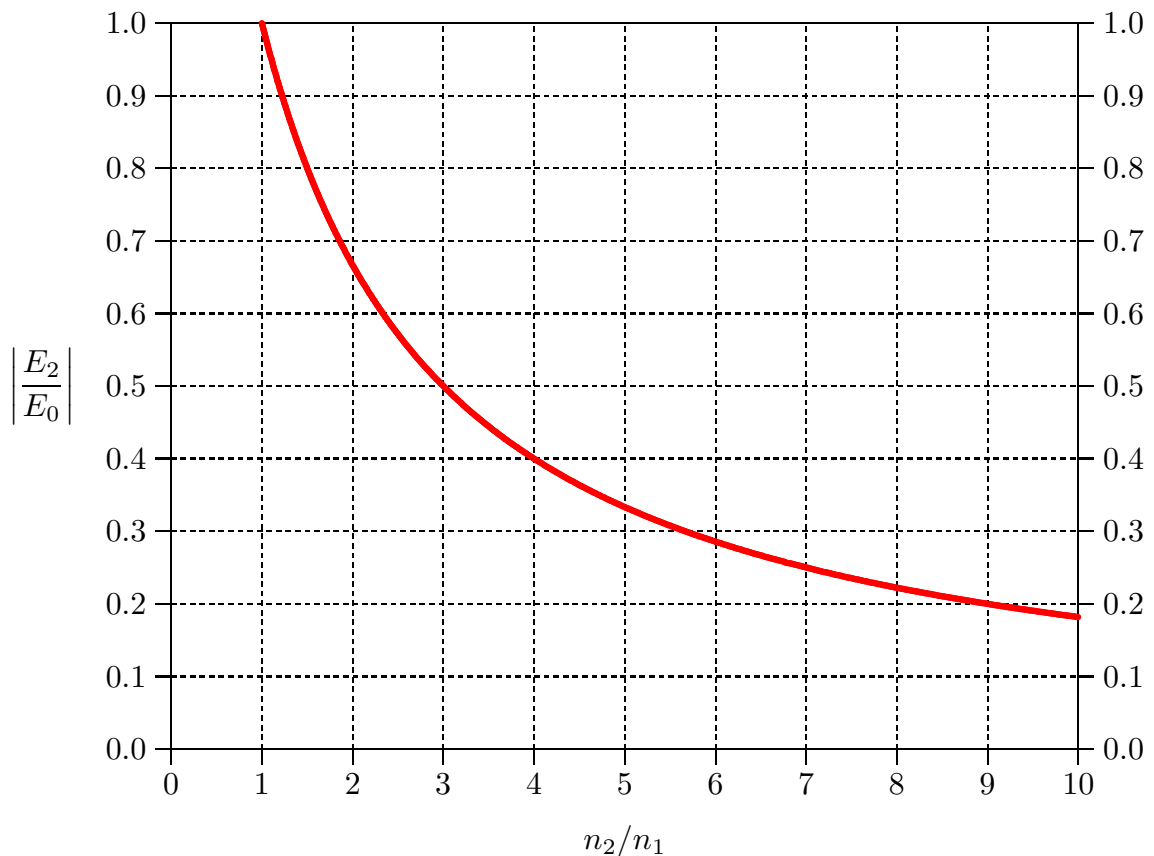
**Tutti i diagrammi presentano massimi relativi ogni  $36^\circ$  a partire da zero e, ovviamente, minimi relativi ogni  $36^\circ$  a partire da  $18^\circ$ . Ricordiamo che l'angolo che sottende ciascun lato di un pentagono regolare é  $72^\circ$ .**

**11-27) Esercizio n. 3 del 7/10/2011**

Un'onda elettromagnetica piana, viaggiante in un mezzo dielettrico (perfetto) di indice di rifrazione  $n_1$ , incide, in direzione della normale, su un mezzo dielettrico (perfetto) di indice di rifrazione  $n_2 > n_1$ . Graficare, in funzione del rapporto  $n_2/n_1$  da 1 a 10: a) il rapporto fra il modulo del campo elettrico trasmesso e quello incidente; b) il rapporto fra il modulo del campo magnetico trasmesso e quello incidente.

$$E_2 = \frac{2n_1}{n_1 + n_2} E_0 = \frac{2}{\left(1 + \frac{n_2}{n_1}\right)} E_0$$

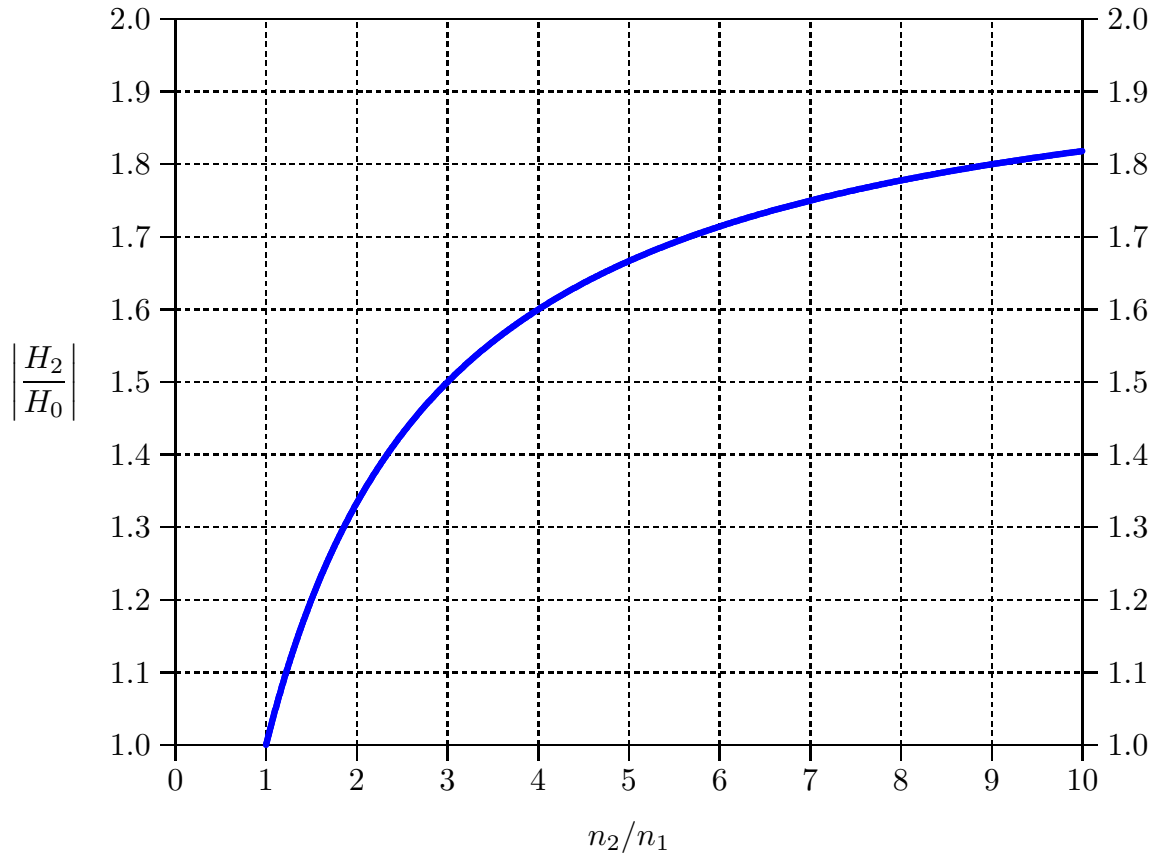
**Rapporto fra il modulo del campo elettrico trasmesso e quello incidente per incidenza normale in funzione di  $\frac{n_2}{n_1}$**



$n_2/n_1$	1	2	3	4	5	6	7	8	9	10
$\left \frac{E_2}{E_0}\right $	1	0.6667	0.5000	0.4000	0.3333	0.2857	0.2500	0.2222	0.2000	0.1818

$$H_2 = \frac{2n_2}{n_1 + n_2} H_0 = \frac{2 \frac{n_2}{n_1}}{\left(1 + \frac{n_2}{n_1}\right)} H_0$$

Rapporto fra il modulo del campo magnetico trasmesso e quello incidente per incidenza normale in funzione di  $\frac{n_2}{n_1}$



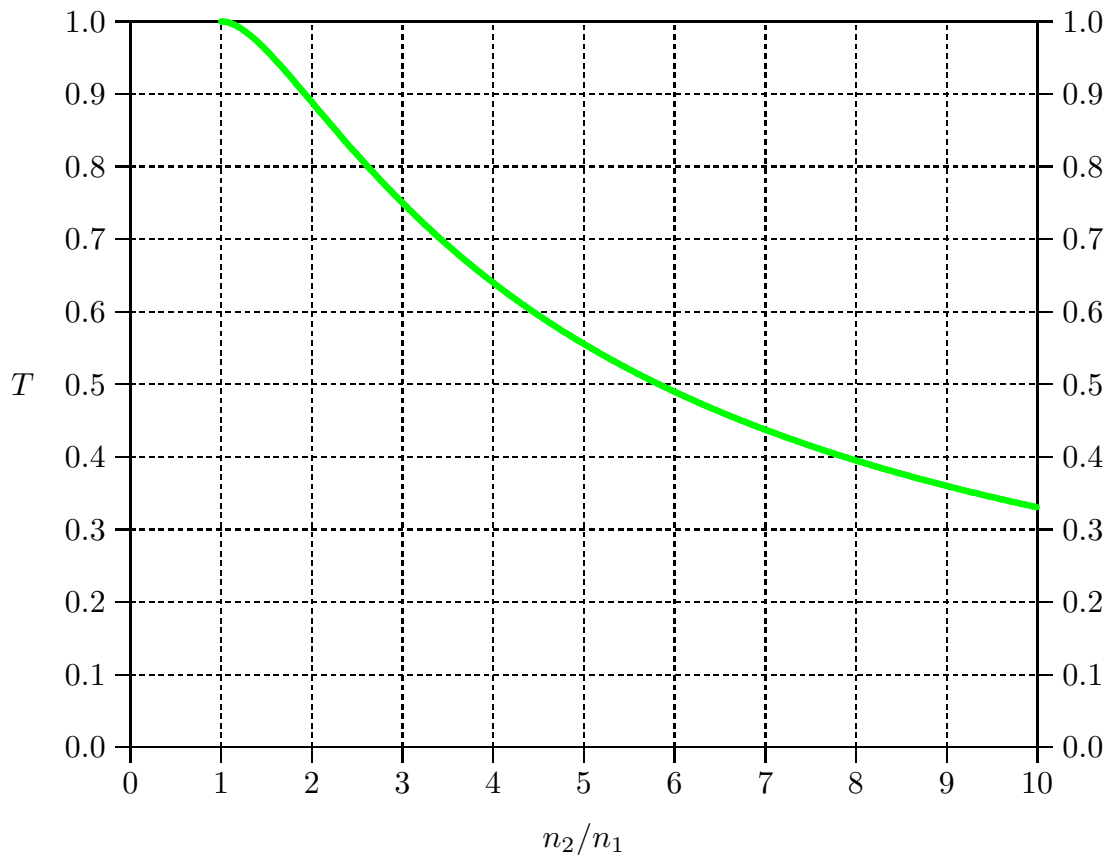
$n_2/n_1$	1	2	3	4	5	6	7	8	9	10
$\left \frac{H_2}{H_0}\right $	1	1.3333	1.5000	1.6000	1.6667	1.7143	1.7500	1.7778	1.8000	1.8182

**11-28) Esercizio n. 4 del 7/10/2011**

Con riferimento al problema precedente, graficare il coefficiente di trasmissione in funzione  $n_2/n_1$ .

$$T = \frac{n_2}{n_1} \frac{|E_2|^2}{|E_0|^2} = \frac{n_2}{n_1} \left[ \frac{2}{\left(1 + \frac{n_2}{n_1}\right)} \right]^2$$

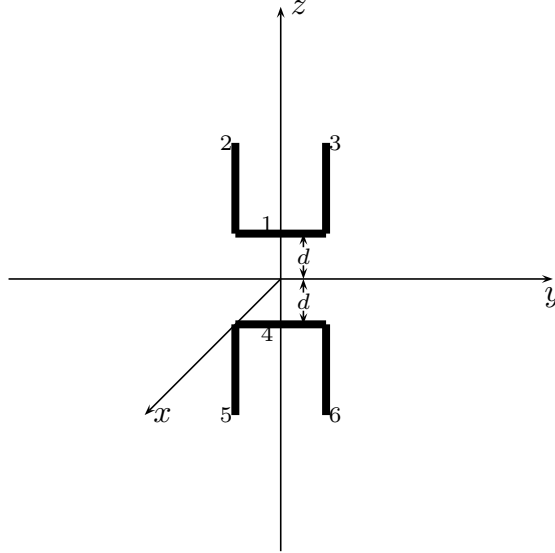
**Coefficiente di trasmissione per  
incidenza normale in funzione di  $\frac{n_2}{n_1}$**



$n_2/n_1$	1	2	3	4	5	6	7	8	9	10
$T$	1	0.8889	0.7500	0.6400	0.5556	0.4898	0.4375	0.3951	0.3600	0.3306

**11-29) Esercizio n. 1 del 4/11/2011**

Sia dato un sistema di 6 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate come in figura. Determinare l'espressione del vettore di Poynting irradiato.



(vedi es. n.1 del 27/11/2009 ed es. n.1 del 5/11/2010)

Le densità di corrente sull'antenna 1, sull'antenna 2, sull'antenna 3, sull'antenna 4, sull'antenna 5 e sull'antenna 6 sono rispettivamente:

$$\left\{ \begin{array}{ll} \vec{J}^{(1)} = \hat{y}A_1\delta(x)\delta(z - z_1) \cos k(y - y_1) & y_1 - l \leq y \leq y_1 + l \\ \vec{J}^{(2)} = \hat{z}A_2\delta(x)\delta(y - y_2) \cos k(z - z_2) & z_2 - l \leq z \leq z_2 + l \\ \vec{J}^{(3)} = \hat{z}A_3\delta(x)\delta(y - y_3) \cos k(z - z_3) & z_3 - l \leq z \leq z_3 + l \\ \vec{J}^{(4)} = \hat{y}A_4\delta(x)\delta(z - z_4) \cos k(y - y_4) & y_4 - l \leq y \leq y_4 + l \\ \vec{J}^{(5)} = \hat{z}A_5\delta(x)\delta(y - y_5) \cos k(z - z_5) & z_5 - l \leq z \leq z_5 + l \\ \vec{J}^{(6)} = \hat{z}A_6\delta(x)\delta(y - y_6) \cos k(z - z_6) & z_6 - l \leq z \leq z_6 + l \end{array} \right.$$

Posto  $A_1 = A_2 = A_3 = A_4 = A_5 = A_6 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante é la somma delle sei:

$$\begin{aligned} \vec{J} = & \hat{y}\delta(x)\delta(z - z_1) \cos k(y - y_1) + \hat{z}\delta(x)\delta(y - y_2) \cos k(z - z_2) + \\ & + \hat{z}\delta(x)\delta(y - y_3) \cos k(z - z_3) + \hat{y}\delta(x)\delta(z - z_4) \cos k(y - y_4) + \\ & + \hat{z}\delta(x)\delta(y - y_5) \cos k(z - z_5) + \hat{z}\delta(x)\delta(y - y_6) \cos k(z - z_6) \end{aligned}$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  é:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}') d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{y} \delta(x') \delta(z' - z_1) \cos k(y' - y_1) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y' - y_2) \cos k(z' - z_2) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y' - y_3) \cos k(z' - z_3) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{y} \delta(x') \delta(z' - z_4) \cos k(y' - y_4) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y' - y_5) \cos k(z' - z_5) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y' - y_6) \cos k(z' - z_6) dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{y} e^{-ikz_1 \cos \theta} \int_{y_1-l}^{y_1+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_1) dy' + \\ & + \hat{z} e^{-iky_2 \sin \theta \sin \phi} \int_{z_2-l}^{z_2+l} e^{-ikz' \cos \theta} \cos k(z' - z_2) dz' + \\ & + \hat{z} e^{-iky_3 \sin \theta \sin \phi} \int_{z_3-l}^{z_3+l} e^{-ikz' \cos \theta} \cos k(z' - z_3) dz' + \\ & + \hat{y} e^{-ikz_4 \cos \theta} \int_{y_4-l}^{y_4+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_4) dy' + \\ & + \hat{z} e^{-iky_5 \sin \theta \sin \phi} \int_{z_6-l}^{z_6+l} e^{-ikz' \cos \theta} \cos k(z' - z_5) dz' + \\ & + \hat{z} e^{-iky_6 \sin \theta \sin \phi} \int_{z_6-l}^{z_6+l} e^{-ikz' \cos \theta} \cos k(z' - z_6) dz' \end{aligned}$$

Valutiamo  $\int_{z_i-l}^{z_i+l} e^{-ikz' \cos \theta} \cos k(z' - z_i) dz'$ .

Poniamo  $z' - z_i = u \implies dz' = du$ . Per  $z' = z_i - l \implies u = -l$ . Per  $z' = z_i + l \implies u = +l$ . Si ha, quindi:

$$\int_{z_i-l}^{z_i+l} e^{-ikz'} \cos \theta \cos k(z' - z_i) dz' = e^{-ikz_i} \cos \theta \int_{-l}^{+l} e^{-iku} \cos \theta \cos kudu =$$

$$= e^{-ikz_i} \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta}$$

Analogamente valutiamo  $\int_{y_i-l}^{y_i+l} e^{-iky'} \sin \theta \sin \phi \cos k(y' - y_i) dy'$ .

Poniamo  $y' - y_i = u \implies dy' = du$ . Per  $y' = y_i - l \implies u = -l$ . Per  $y' = y_i + l \implies u = +l$ . Si ha, quindi:

$$\int_{y_i-l}^{y_i+l} e^{-iky'} \sin \theta \sin \phi \cos k(y' - y_i) dy' =$$

$$= e^{-iky_i} \sin \theta \sin \phi \int_{-l}^{+l} e^{-iku} \sin \theta \sin \phi \cos kudu = e^{-iky_i} \sin \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi}$$

avendo calcolato:

$$\int_{-l}^{+l} e^{-iku} \sin \theta \sin \phi \cos kudu = \int_{-l}^{+l} e^{-iku} \cos \chi \cos kudu = \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi}$$

in quanto:

$$\hat{y} \cdot \hat{r} = \cos \chi = \sin \theta \sin \phi$$

essendo  $\chi$  l'angolo formato fra l'asse  $y$  e la direzione del vettore posizione  $\hat{e}_r$ .

Ne segue:

$$\vec{N}(\theta, \phi) = \hat{y} e^{-ikz_1} \cos \theta e^{-iky_1} \sin \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} +$$

$$+ \hat{z} e^{-iky_2} \sin \theta \sin \phi e^{-ikz_2} \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} +$$

$$+ \hat{z} e^{-iky_3} \sin \theta \sin \phi e^{-ikz_3} \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} +$$

$$+ \hat{y} e^{-ikz_4} \cos \theta e^{-iky_4} \sin \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} +$$

$$+ \hat{z} e^{-iky_5} \sin \theta \sin \phi e^{-ikz_5} \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} +$$

$$+ \hat{z} e^{-iky_6} \sin \theta \sin \phi e^{-ikz_6} \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta}$$



$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{y} \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{k \left(1 - \sin^2 \theta \sin^2 \phi\right)} \left[ e^{-ikz_1 \cos \theta} e^{-iky_1 \sin \theta \sin \phi} + \right. \\ & \left. + e^{-ikz_4 \cos \theta} e^{-iky_4 \sin \theta \sin \phi} \right] + \\ & + \hat{z} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \left[ e^{-iky_2 \sin \theta \sin \phi} e^{-ikz_2 \cos \theta} + \right. \\ & + e^{-iky_3 \sin \theta \sin \phi} e^{-ikz_3 \cos \theta} + e^{-iky_5 \sin \theta \sin \phi} e^{-ikz_5 \cos \theta} + \\ & \left. + e^{-iky_6 \sin \theta \sin \phi} e^{-ikz_6 \cos \theta} \right] \end{aligned}$$

Si ha:

$$\left\{ \begin{array}{ll} y_1 = 0; & z_1 = +d \\ y_2 = -\frac{\lambda}{4}; & z_2 = +d + \frac{\lambda}{4} \\ y_3 = +\frac{\lambda}{4}; & z_3 = +d + \frac{\lambda}{4} \\ y_4 = 0; & z_4 = -d \\ y_5 = -\frac{\lambda}{4}; & z_5 = -d - \frac{\lambda}{4} \\ y_6 = +\frac{\lambda}{4}; & z_6 = -d - \frac{\lambda}{4} \end{array} \right.$$

Quindi:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{y} \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{k \left(1 - \sin^2 \theta \sin^2 \phi\right)} \left[ e^{-ikd \cos \theta} + e^{+ikd \cos \theta} \right] + \\ & + \hat{z} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \left[ e^{+ik\frac{\lambda}{4} \sin \theta \sin \phi} e^{-ik\left(+d + \frac{\lambda}{4}\right) \cos \theta} + \right. \\ & + e^{-ik\frac{\lambda}{4} \sin \theta \sin \phi} e^{-ik\left(+d + \frac{\lambda}{4}\right) \cos \theta} + \\ & + e^{+ik\frac{\lambda}{4} \sin \theta \sin \phi} e^{-ik\left(-d - \frac{\lambda}{4}\right) \cos \theta} + \\ & \left. + e^{-ik\frac{\lambda}{4} \sin \theta \sin \phi} e^{-ik\left(-d - \frac{\lambda}{4}\right) \cos \theta} \right] \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{y} \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{k \left(1 - \sin^2 \theta \sin^2 \phi\right)} \left[ 2 \cos(kd \cos \theta) \right] + \\ & + \hat{z} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \left[ 2 \cos\left(k \frac{\lambda}{4} \sin \theta \sin \phi\right) e^{-ik \left(+d + \frac{\lambda}{4}\right) \cos \theta} + \right. \\ & \left. + 2 \cos\left(k \frac{\lambda}{4} \sin \theta \sin \phi\right) e^{-ik \left(-d - \frac{\lambda}{4}\right) \cos \theta} \right] \end{aligned}$$

e, ancora:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{y} \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{k \left(1 - \sin^2 \theta \sin^2 \phi\right)} \left[ 2 \cos(kd \cos \theta) \right] + \\ & + \hat{z} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \left\{ 2 \cos\left(k \frac{\lambda}{4} \sin \theta \sin \phi\right) 2 \cos\left[k \left(+d + \frac{\lambda}{4}\right) \cos \theta\right] \right\} \end{aligned}$$

In definitiva:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{y} \frac{2 \cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{k \left(1 - \sin^2 \theta \sin^2 \phi\right)} \left[ 2 \cos(kd \cos \theta) \right] + \\ & + \hat{z} \frac{2 \cos\left(\frac{\pi}{2} \cos \theta\right)}{k \sin^2 \theta} \left\{ 4 \cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right) \cos\left[\left(+kd + \frac{\pi}{2}\right) \cos \theta\right] \right\} \end{aligned}$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \left\{ \sin \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ 2 \cos (kd \cos \theta) \right] + \right. \\
 & + \cos \theta \frac{2 \cos \left( \frac{\pi}{2} \cos \theta \right)}{k \sin^2 \theta} \left\{ 4 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right) \cos \left[ \left( +kd + \frac{\pi}{2} \right) \cos \theta \right] \right\} + \\
 & + \hat{e}_\theta \left\{ \cos \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ 2 \cos (kd \cos \theta) \right] - \right. \\
 & \left. - \sin \theta \frac{2 \cos \left( \frac{\pi}{2} \cos \theta \right)}{k \sin^2 \theta} \left[ 4 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right) \cos \left[ \left( +kd + \frac{\pi}{2} \right) \cos \theta \right] \right] \right\} + \\
 & + \hat{e}_\phi \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ 2 \cos (kd \cos \theta) \right]
 \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

essendo:

$$\begin{aligned}
 N_\theta(\theta, \phi) = & \left\{ \cos \theta \sin \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ 2 \cos (kd \cos \theta) \right] - \right. \\
 & \left. - \sin \theta \frac{2 \cos \left( \frac{\pi}{2} \cos \theta \right)}{k \sin^2 \theta} \left[ 4 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right) \cos \left[ \left( +kd + \frac{\pi}{2} \right) \cos \theta \right] \right] \right\} \\
 N_\phi(\theta, \phi) = & \cos \phi \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \left[ 2 \cos (kd \cos \theta) \right]
 \end{aligned}$$

**11-30) Esercizio n. 2 del 4/11/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\phi = 0^\circ$  ( $xz$ ). Si ponga  $d = \frac{\lambda}{4}$ .

$$|N_\theta(\theta, \phi)|_{(\phi=0^\circ)}^2 = \frac{16}{k^2} \left[ 2 \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \cos \left[ \left( +kd + \frac{\pi}{2} \right) \cos \theta \right] \right]^2$$

$$|N_\phi(\theta, \phi)|_{(\phi=0^\circ)}^2 = \frac{16}{k^2} \left[ \cos(kd \cos \theta) \right]^2$$

Quindi:

$$\begin{aligned} \langle \vec{S} \rangle_{(\phi=0^\circ)} &= \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta(\theta, \phi)|_{(\phi=0^\circ)}^2 + |N_\phi(\theta, \phi)|_{(\phi=0^\circ)}^2 \right) \hat{e}_r = \\ &= \frac{1}{2} Z \left( \frac{1}{\pi r} \right)^2 \left\{ \left[ 2 \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \cos \left[ \left( +kd + \frac{\pi}{2} \right) \cos \theta \right] \right]^2 + \left[ \cos(kd \cos \theta) \right]^2 \right\} \end{aligned}$$

Grafichiamo il fattore di forma per  $d = \frac{\lambda}{4} \implies kd = \frac{\pi}{2}$ .

$$F(\theta) = \left[ 2 \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} \cos(\pi \cos \theta) \right]^2 + \left[ \cos\left(\frac{\pi}{2} \cos \theta\right) \right]^2$$

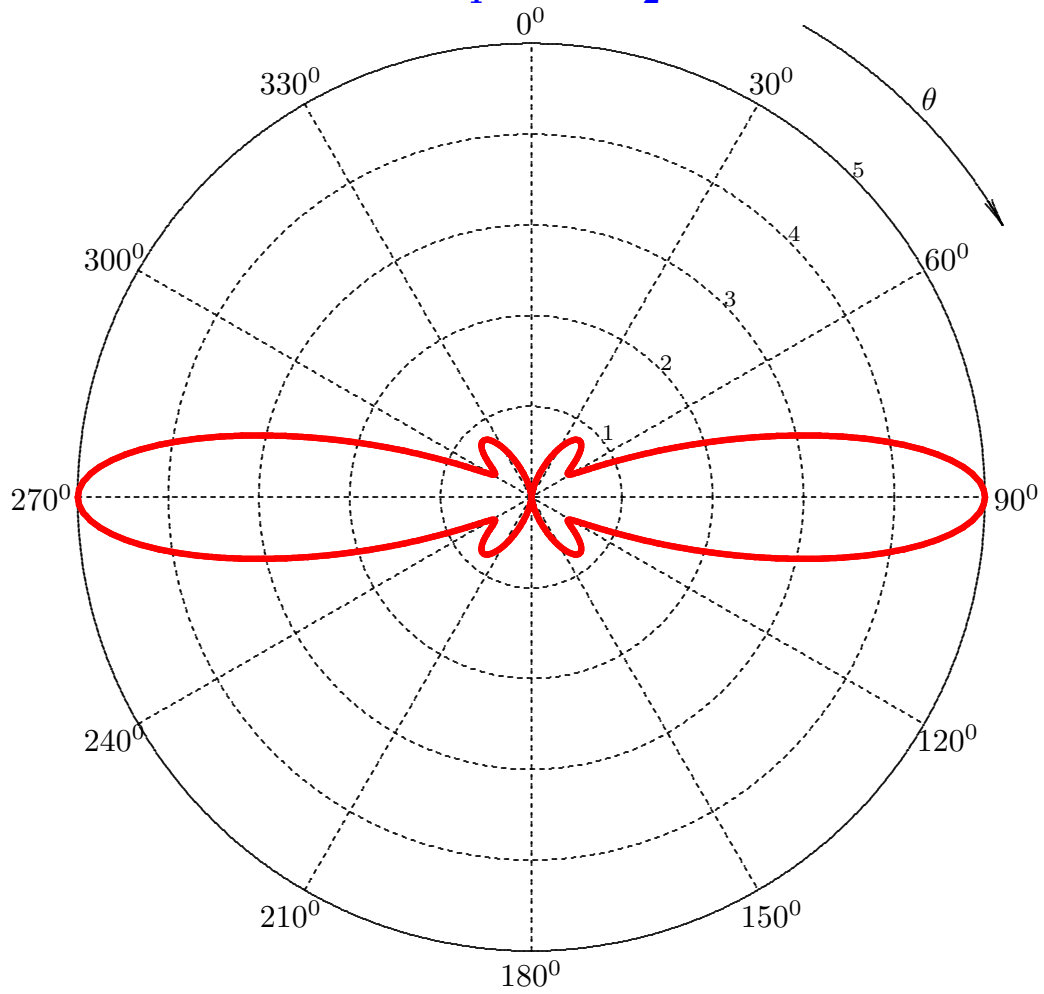
Si ha:

$$\lim_{\theta \rightarrow 0^\circ} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta} = 0$$

$F(\theta)$  si annulla per  $\theta = 0^\circ$ .

Diagramma di radiazione per  $\phi = 0^\circ$

$$d = \frac{\lambda}{4} \Rightarrow kd = \frac{\pi}{2}$$



**11-31) Esercizio n. 3 del 4/11/2011**

Un fascetto di radiazione ultravioletta di lunghezza d'onda relativa al vuoto  $\lambda_0 = 0.1078 \mu m$ , viaggiante in aria, incide, in direzione della normale, su un sottilissimo strato d'argento, di spessore  $d = 0.01 \mu m$ , depositato su vetro. I parametri costitutivi dell'argento competenti alla lunghezza d'onda data sono:

$$n_r = 1.3, \quad n_i = 0.573, \quad \mu_r = 1$$

L'indice di riflessione del vetro é  $n_3 = 1.5$  (trascurando la parte immaginaria).  
Calcolare il coefficiente di riflessione.

Il sistema può essere considerato come una lamina piana assorbente (argento) posta fra l'aria e il vetro.

Dalla teoria delle lamine piane assorbenti si deduce che il coefficiente di riflessione é:

$$R = \frac{|r_{12}|^2 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}^* r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}^* r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12} r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12} r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) \right] + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)}}$$

Cominciamo con il calcolare alcune quantità che servono per la valutazione dei coefficienti che figurano nella formula della riflettività.:

$$(n_1 - n_r) = (1 - 1.3) = -0.3; \quad (n_1 + n_r) = (1 + 1.3) = 2.3$$

$$(n_r - n_3) = (1.3 - 1.5) = -0.2; \quad (n_r + n_3) = (1.3 + 1.5) = 2.8$$

$$[(n_1 - n_r)(n_1 + n_r) - n_i^2] = -0.3 \cdot 2.3 - (0.573)^2 = -1.0183$$

$$[(n_r - n_3)(n_r + n_3) + n_i^2] = -0.2 \cdot 2.8 + (0.573)^2 = -0.2317$$

$$[(n_1 + n_r)^2 + n_i^2] = (2.3)^2 + (0.573)^2 = 5.6183$$

$$[(n_1 - n_r)^2 + n_i^2] = (-0.3)^2 + (0.573)^2 = 0.4183$$

$$[(n_r + n_3)^2 + n_i^2] = (2.8)^2 + (0.573)^2 = 8.1683$$

$$[(n_r - n_3)^2 + n_i^2] = (-0.2)^2 + (0.573)^2 = 0.3683$$

$$4n_i^2 n_1 n_3 = 4 \cdot (0.573)^2 \cdot 1.5 = 1.9700$$

$$\Re(r_{12}^* r_{23}) = \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] - 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq$$

$$\simeq \frac{(-1.0183)(-0.2317) - 1.9700}{5.6183 \cdot 8.1683} \simeq -\frac{1.7341}{45.8920} \simeq -0.0378$$

$$\Im(r_{12}^* r_{23}) = \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] + 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq$$

$$\simeq \frac{2 \cdot 0.573 \cdot 1.5 \cdot (-1.0183) + 2 \cdot 0.573 \cdot (-0.2317)}{45.8920} \simeq$$

$$\simeq \frac{-1.7505 - 0.2655}{45.8920} \simeq -\frac{2.0160}{45.8920} \simeq -0.0439$$

$$\Re(r_{12} r_{23}) = \frac{[(n_1 - n_r)(n_1 + n_r) - n_i^2] [(n_r - n_3)(n_r + n_3) + n_i^2] + 4n_i^2 n_1 n_3}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq$$

$$\simeq \frac{(-1.0183)(-0.2317) + 1.9700}{45.820} \simeq \frac{2.2059}{45.820} \simeq +0.0481$$

$$\Im(r_{12} r_{23}) = \frac{2n_i n_3 [(n_1 - n_r)(n_1 + n_r) - n_i^2] - 2n_i n_1 [(n_r - n_3)(n_r + n_3) + n_i^2]}{[(n_1 + n_r)^2 + n_i^2] [(n_r + n_3)^2 + n_i^2]} \simeq$$

$$\simeq \frac{-1.7505 + 0.2655}{45.8920} \simeq -\frac{1.4850}{45.8920} \simeq -0.0324$$

Inoltre:

$$\Re(r_{12}) = \frac{n_1^2 - n_r^2 - n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{1.0183}{5.6183} \simeq -0.1812$$

$$\Re(r_{23}) = \frac{n_r^2 - n_3^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq -\frac{0.2317}{8.1683} \simeq -0.0284$$

$$\Im(r_{12}) = \frac{-2n_i n_1}{(n_1 + n_r)^2 + n_i^2} \simeq -\frac{1.1460}{5.6183} \simeq -0.2040$$

$$\Im(r_{23}) = \frac{2n_i n_3}{(n_r + n_3)^2 + n_i^2} \simeq \frac{1.7190}{8.1683} \simeq +0.2104$$

$$|r_{12}|^2 = \frac{(n_1 - n_r)^2 + n_i^2}{(n_1 + n_r)^2 + n_i^2} \simeq \frac{0.4183}{5.6183} \simeq +0.0745$$

$$|r_{23}|^2 = \frac{(n_r - n_3)^2 + n_i^2}{(n_r + n_3)^2 + n_i^2} \simeq \frac{0.3683}{8.1683} \simeq +0.0451$$

$$\sin\left(4\pi n_r \frac{d}{\lambda_0}\right) = \sin\left(4\pi \cdot 1.3 \frac{0.01}{0.1078}\right) \simeq +0.9985$$

$$\cos\left(4\pi n_r \frac{d}{\lambda_0}\right) = \sin\left(4\pi \cdot 1.3 \frac{0.01}{0.1078}\right) \simeq +0.0553$$

$$\exp\left[-\left(4\pi n_i \frac{d}{\lambda_0}\right)\right] \simeq \exp\left[-\left(4\pi \cdot 0.573 \frac{0.01}{0.1078}\right)\right] \simeq \exp(-0.6680) \simeq 0.5127$$

$$\exp \left[ - \left( 8\pi n_i \frac{d}{\lambda_0} \right) \right] \simeq \exp \left[ - \left( 8\pi \cdot 0.573 \frac{0.01}{0.1078} \right) \right] \simeq \exp(-1.3359) \simeq 0.2629$$

Quindi:

$$R = \frac{0.0745 + 0.5127 \cdot [2 \cdot (-0.0378) \cdot 0.0553 - 2 \cdot (-0.0439) \cdot 0.9985] + 0.0119}{1 + 0.5127[2(0.0481)(0.0553) - 2(-0.0324)(0.9985)] + 8.8333 \cdot 10^{-4}} \simeq$$

$$\simeq \frac{0.1292}{1.0368} \simeq \underline{\underline{0.1247}} \simeq \underline{\underline{12.47\%}}$$



**11-32) Esercizio n. 4 del 4/11/2011**

Con riferimento al problema precedente si valuti il coefficiente di trasmissione.

Poiché risulta, in questo caso:

$$\frac{\beta_3 \mu_1}{\beta_1 \mu_3} = \frac{n_3}{n_1}$$

il coefficiente di trasmissione é:

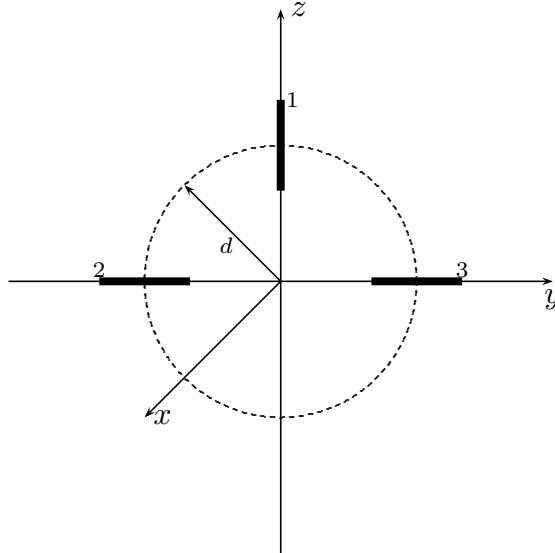
$$T = \frac{\frac{n_3}{n_1} [1 + 2\Re(r_{12}) + |r_{12}|^2] [1 + 2\Re(r_{23}) + |r_{23}|^2] e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)}}{1 + e^{-\left(4\pi n_i \frac{d}{\lambda_0}\right)} \left[ 2\Re(r_{12}r_{23}) \cos\left(4\pi n_r \frac{d}{\lambda_0}\right) - 2\Im(r_{12}r_{23}) \sin\left(4\pi n_r \frac{d}{\lambda_0}\right) + |r_{12}|^2 |r_{23}|^2 e^{-\left(8\pi n_i \frac{d}{\lambda_0}\right)} \right]}$$

Poiché il coefficiente di trasmissione ha lo stesso denominatore del coefficiente di riflessione, procediamo al calcolo del solo numeratore. Si ha:

$$T = \frac{1.5 \cdot [1 + 2 \cdot (-0.1812) + 0.0745] \cdot [1 + 2 \cdot (-0.0284) + 0.0451] \cdot 0.5127}{1.0368} \simeq \frac{0.5412}{1.0368} \simeq \underline{\underline{0.5220}} \simeq \underline{\underline{52.2\%}}$$

**11-33) Esercizio n. 1 del 9/12/2011**

Sia dato un sistema di 3 antenne a mezz'onda uniformemente alimentate e con le correnti in fase fra di loro. Esse sono posizionate con i loro centri nel piano  $yz$ . Le correnti sono orientate come in figura. Determinare l'espressione del vettore di Poynting irradiato.



Le densità di corrente sull'antenna 1, sull'antenna 2 e sull'antenna 3 sono rispettivamente:

$$\begin{cases} \vec{J}^{(1)} = \hat{z}A_1\delta(x)\delta(y) \cos k(z - z_1) & z_1 - l \leq z \leq z_1 + l \\ \vec{J}^{(2)} = \hat{y}A_2\delta(x)\delta(z) \cos k(y - y_2) & y_2 - l \leq y \leq y_2 + l \\ \vec{J}^{(3)} = \hat{y}A_3\delta(x)\delta(z) \cos k(y - y_3) & y_3 - l \leq y \leq y_3 + l \end{cases}$$

Posto  $A_1 = A_2 = A_3 = 1$  per la uniformità del sistema di antenne, la densità di corrente risultante è la somma delle tre:

$$\vec{J} = \hat{z}\delta(x)\delta(y) \cos k(z - z_1) + \hat{y}\delta(x)\delta(z) \cos k(y - y_2) + \hat{y}\delta(x)\delta(z) \cos k(y - y_3)$$

Il vettore di radiazione (far field)  $\vec{N}(\theta, \phi)$  è:

$$\vec{N}(\theta, \phi) = \int_V e^{-ik\hat{e}_r \cdot \vec{r}'} \vec{J}(\vec{r}')d^3r'$$

Ora:

$$\hat{e}_r = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$$

Quindi:

$$\hat{e}_r \cdot \vec{r}' = x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta$$

Ne segue:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \\ = & \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{z} \delta(x') \delta(y') \cos k(z' - z_1) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{y} \delta(x') \delta(z') \cos k(y' - y_2) dx' dy' dz' + \\ & + \int_V e^{-ik(x' \sin \theta \cos \phi + y' \sin \theta \sin \phi + z' \cos \theta)} \hat{y} \delta(x') \delta(z') \cos k(y' - y_3) dx' dy' dz' \end{aligned}$$

ossia:

$$\begin{aligned} \vec{N}(\theta, \phi) = & \hat{z} \int_{z_1-l}^{z_1+l} e^{-ikz' \cos \theta} \cos k(z' - z_1) dz' + \\ & + \hat{y} \int_{y_2-l}^{y_2+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_2) dy' + \\ & + \hat{y} \int_{y_3-l}^{y_3+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_3) dy' \end{aligned}$$

Valutiamo  $\int_{y_i-l}^{y_i+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_i) dy'$ .

Poniamo  $y' - y_i = u \implies dy' = du$ . Per  $y' = y_i - l \implies u = -l$ . Per  $y' = y_i + l \implies u = +l$ . Si ha, quindi:

$$\begin{aligned} & \int_{y_i-l}^{y_i+l} e^{-iky' \sin \theta \sin \phi} \cos k(y' - y_i) dy' = \\ = & e^{-iky_i \sin \theta \sin \phi} \int_{-l}^{+l} e^{-iku \sin \theta \sin \phi} \cos kudu = e^{-iky_i \sin \theta \sin \phi} \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)} \end{aligned}$$

avendo calcolato:

$$\int_{-l}^{+l} e^{-iku \sin \theta \sin \phi} \cos kudu = \int_{-l}^{+l} e^{-iku \cos \chi} \cos kudu = \frac{2 \cos \left( \frac{\pi}{2} \sin \theta \sin \phi \right)}{k \left( 1 - \sin^2 \theta \sin^2 \phi \right)}$$

in quanto:

$$\hat{y} \cdot \hat{r} = \cos \chi = \sin \theta \sin \phi$$

essendo  $\chi$  l'angolo formato fra l'asse  $y$  e la direzione del vettore posizione  $\hat{e}_r$ .

Analogamente valutiamo  $\int_{z_i-l}^{z_i+l} e^{-ikz' \cos \theta} \cos k(z' - z_i) dz'$ .

Poniamo  $z' - z_i = u \implies dz' = du$ . Per  $z' = z_i - l \implies u = -l$ . Per  $z' = z_i + l \implies u = +l$ . Si ha, quindi:

$$\int_{z_i-l}^{z_i+l} e^{-ikz' \cos \theta} \cos k(z' - z_i) dz' = e^{-ikz_i \cos \theta} \int_{-l}^{+l} e^{-iku \cos \theta} \cos kudu =$$

$$= e^{-ikz_i \cos \theta} \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta}$$

Ne segue:

$$\vec{N}(\theta, \phi) = \hat{z} e^{-ikz_1 \cos \theta} \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} +$$

$$+ \hat{y} e^{-iky_2 \sin \theta \sin \phi} \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} +$$

$$+ \hat{y} e^{-iky_3 \sin \theta \sin \phi} \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi}$$

che si può meglio scrivere:

$$\vec{N}(\theta, \phi) = \hat{z} \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} e^{-ikz_1 \cos \theta} +$$

$$+ \hat{y} \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_3 \sin \theta \sin \phi} \right]$$

Poiché:

$$\begin{cases} \hat{x} = \hat{e}_r \sin \theta \cos \phi + \hat{e}_\theta \cos \theta \cos \phi - \hat{e}_\phi \sin \phi \\ \hat{y} = \hat{e}_r \sin \theta \sin \phi + \hat{e}_\theta \cos \theta \sin \phi + \hat{e}_\phi \cos \phi \\ \hat{z} = \hat{e}_r \cos \theta - \hat{e}_\theta \sin \theta \end{cases}$$

si ha:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \left\{ \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} e^{-ikz_1 \cos \theta} + \right. \\
 & \left. + \sin \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_3 \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\theta \left\{ -\sin \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} e^{-ikz_1 \cos \theta} + \right. \\
 & \left. + \cos \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_3 \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\phi \left\{ \cos \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{-iky_2 \sin \theta \sin \phi} + e^{-iky_3 \sin \theta \sin \phi} \right] \right\}
 \end{aligned}$$

Dalla figura risulta:

$$z_1 = +d, \quad y_2 = -d, \quad y_3 = +d$$

Quindi:

$$\begin{aligned}
 \vec{N}(\theta, \phi) = & \hat{e}_r \left\{ \cos \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} e^{-ikd \cos \theta} + \right. \\
 & \left. + \sin \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{+ikd \sin \theta \sin \phi} + e^{-ikd \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\theta \left\{ -\sin \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} e^{-ikd \cos \theta} + \right. \\
 & \left. + \cos \theta \sin \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{+ikd \sin \theta \sin \phi} + e^{-ikd \sin \theta \sin \phi} \right] \right\} + \\
 & + \hat{e}_\phi \left\{ \cos \phi \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \left[ e^{+ikd \sin \theta \sin \phi} + e^{-ikd \sin \theta \sin \phi} \right] \right\}
 \end{aligned}$$

Il vettore di Poynting (far field), mediato in un periodo, é:

$$\langle \vec{S} \rangle = \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|^2 + |N_\phi|^2 \right) \hat{e}_r$$

Si ha:

$$N_{\theta}(\theta, \phi) = \left\{ -\sin \theta \frac{2}{k} \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} e^{-ikd \cos \theta} + \right. \\ \left. + \cos \theta \sin \phi \frac{4}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \cos(kd \sin \theta \sin \phi) \right\}$$

$$N_{\phi}(\theta, \phi) = \left\{ \cos \phi \frac{4}{k} \frac{\cos\left(\frac{\pi}{2} \sin \theta \sin \phi\right)}{1 - \sin^2 \theta \sin^2 \phi} \cos(kd \sin \theta \sin \phi) \right\}$$

**11-34) Esercizio n. 2 del 9/12/2011**

Con riferimento al problema precedente graficare il diagramma di radiazione nel piano  $\theta = 90^\circ$ . Si ponga  $d = \frac{3}{4}\lambda$ .

Per  $\theta = 90^\circ$  si ha:

$$[N_\theta(\theta, \phi)]_{\theta=90^\circ} = -\frac{2}{k}$$

$$[N_\phi(\theta, \phi)]_{\theta=90^\circ} = \left\{ \cos \phi \frac{4}{k} \frac{\cos\left(\frac{\pi}{2} \sin \phi\right)}{1 - \sin^2 \phi} \cos(kd \sin \phi) \right\}$$

$$\begin{aligned} \langle \vec{S} \rangle_{\theta=90^\circ} &= \frac{1}{2} Z \left( \frac{k}{4\pi r} \right)^2 \left( |N_\theta|_{\theta=90^\circ}^2 + |N_\phi|_{\theta=90^\circ}^2 \right) \hat{e}_r = \\ &= \frac{1}{2} Z \left( \frac{1}{2\pi r} \right)^2 \left\{ 1 + 4 \left[ \frac{\cos\left(\frac{\pi}{2} \sin \phi\right)}{\cos \phi} \cos(kd \sin \phi) \right]^2 \right\} \hat{e}_r \end{aligned}$$

Grafichiamo il fattore di forma:

$$F(\phi) = 1 + 4 \left[ \frac{\cos\left(\frac{\pi}{2} \sin \phi\right)}{\cos \phi} \cos(kd \sin \phi) \right]^2$$

Poniamo  $d = \frac{3}{4}\lambda$  (come in figura)  $\implies kd = \frac{3}{2}\pi$ .

$$F(\phi) = 1 + 4 \left[ \frac{\cos\left(\frac{\pi}{2} \sin \phi\right)}{\cos \phi} \cos\left(\frac{3}{2}\pi \sin \phi\right) \right]^2$$

Si ha:

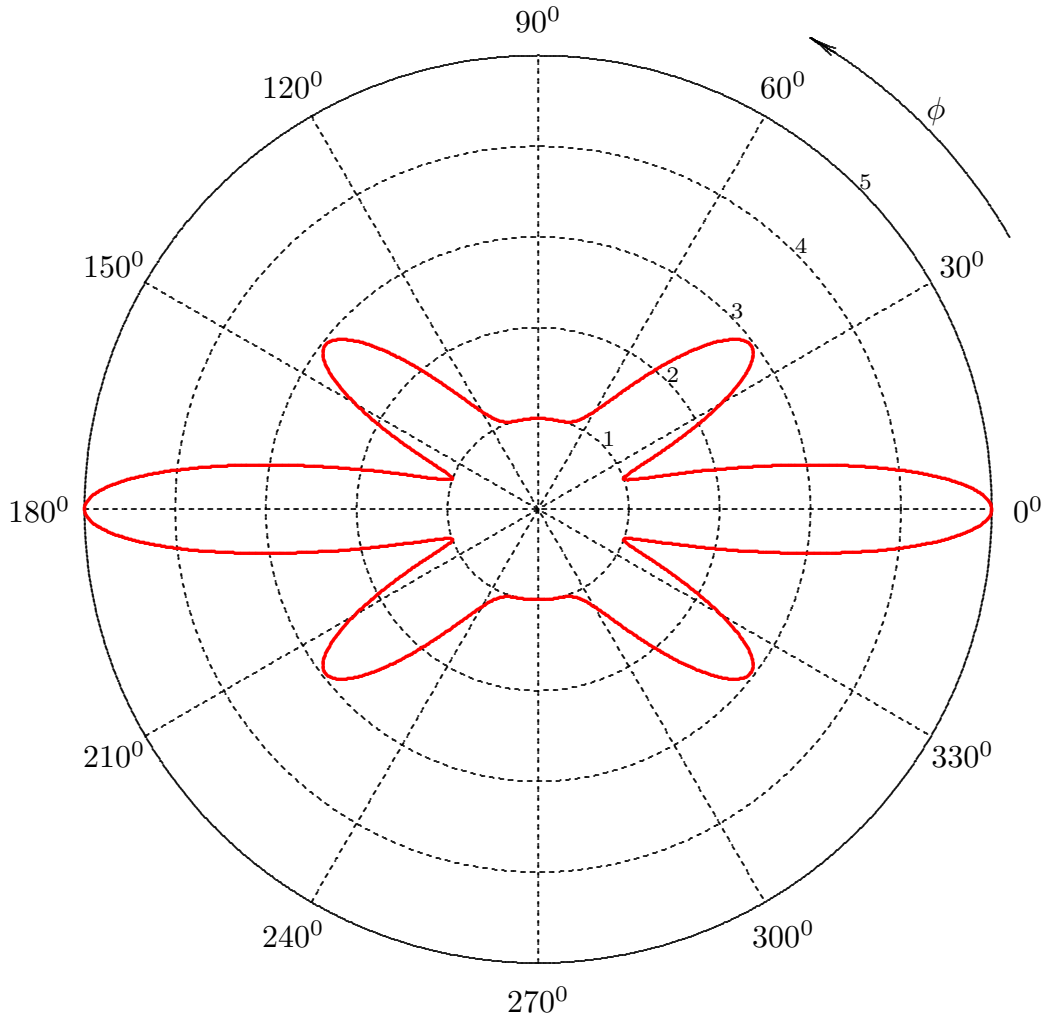
$$\lim_{\phi=90^\circ} \frac{\cos\left(\frac{\pi}{2} \sin \phi\right)}{\cos \phi} = 0$$

Il termine fra parentesi quadre nel fattore di forma si annulla, nel primo quadrante, per  $\phi = 90^\circ$  e per  $\frac{3}{2}\pi \sin \phi = \frac{\pi}{2}$  ossia per  $\sin \phi = \frac{1}{3} \implies \phi = \arcsin\left(\frac{1}{3}\right) = 19^\circ.4712$ .

Quindi per  $\phi_1 \simeq 19^{\circ}.47$  e  $\phi_2 = 90^{\circ}$  il fattore di forma vale 1, che é il valore minimo del diagramma di radiazione. Il valore massimo si ha per  $\phi = 0^{\circ}$  e vale 5.

**Diagramma di radiazione per  $\theta = 90^{\circ}$**

$$d = \frac{3}{4}\lambda \implies kd = \frac{3}{2}\pi$$





**11-35) Esercizio n. 3 del 9/12/2011**

Un fascetto di luce naturale, viaggiante in aria, incide su un mezzo dielettrico perfetto di indice di rifrazione  $n = 1.51$ .

Calcolare i coefficienti di riflessione  $R_{\perp}$ ,  $R_{\parallel}$  e  $R_{nat}$  al variare dell'angolo di incidenza  $\theta_0$ , nonché i coefficienti di trasmissione  $T_{\perp}$ ,  $T_{\parallel}$  e  $T_{nat}$ .

I coefficienti di riflessione per entrambe le polarizzazioni ( $R_{\perp}$  ed  $R_{\parallel}$ ) in funzione dell'angolo di incidenza sono:

$$R_{\perp} = \left| \frac{\sqrt{\epsilon_{r_1}} \cos \theta_0 - \sqrt{\epsilon_{r_2} - \epsilon_{r_1} \sin^2 \theta_0}}{\sqrt{\epsilon_{r_1}} \cos \theta_0 + \sqrt{\epsilon_{r_2} - \epsilon_{r_1} \sin^2 \theta_0}} \right|^2$$

$$R_{\parallel} = \left| \frac{\epsilon_{r_2} \cos \theta_0 - \sqrt{\epsilon_{r_1}} \sqrt{\epsilon_{r_2} - \epsilon_{r_1} \sin^2 \theta_0}}{\epsilon_{r_2} \cos \theta_0 + \sqrt{\epsilon_{r_1}} \sqrt{\epsilon_{r_2} - \epsilon_{r_1} \sin^2 \theta_0}} \right|^2$$

Sostituendo in esse  $\epsilon_{r_1} = 1$  e  $\epsilon_{r_2} = n_2^2$ , otteniamo:

$$R_{\perp} = \left| \frac{\cos \theta_0 - \sqrt{n_2^2 - \sin^2 \theta_0}}{\cos \theta_0 + \sqrt{n_2^2 - \sin^2 \theta_0}} \right|^2$$

$$R_{\parallel} = \left| \frac{n_2^2 \cos \theta_0 - \sqrt{n_2^2 - \sin^2 \theta_0}}{n_2^2 \cos \theta_0 + \sqrt{n_2^2 - \sin^2 \theta_0}} \right|^2$$

$$R_{nat} = \frac{1}{2} R_{\perp} + \frac{1}{2} R_{\parallel}$$

Si ha anche:

$$T_{\perp} = 1 - R_{\perp}$$

$$T_{\parallel} = 1 - R_{\parallel}$$

$$T_{nat} = \frac{1}{2} T_{\perp} + \frac{1}{2} T_{\parallel}$$

Riportiamo in tabella i valori di  $R_{\perp}$ ,  $R_{\parallel}$ ,  $R_{nat}$ ,  $T_{\perp}$ ,  $T_{\parallel}$  e  $T_{nat}$  in funzione di  $\theta_0$ . Osserviamo anche che l'angolo di Brewster é:

$$\theta_B = \arctan \left( \frac{n_2}{n_1} \right) = \arctan(1.51) = 56^{\circ}.4854$$

$\theta_0$	$R_{\perp}$	$T_{\perp}$	$R_{\parallel}$	$T_{\parallel}$	$R_{nat}$	$T_{nat}$
0 <sup>0</sup>	0.0413	0.9587	0.0413	0.9587	0.0413	0.9587
1 <sup>0</sup>	0.0413	0.9587	0.0413	0.9587	0.0413	0.9587
2 <sup>0</sup>	0.0414	0.9586	0.0412	0.9588	0.0413	0.9587
3 <sup>0</sup>	0.0414	0.9586	0.0411	0.9589	0.0413	0.9587
4 <sup>0</sup>	0.0416	0.9584	0.0410	0.9590	0.0413	0.9587
5 <sup>0</sup>	0.0417	0.9583	0.0409	0.9591	0.0413	0.9587
6 <sup>0</sup>	0.0419	0.9581	0.0407	0.9593	0.0413	0.9587
7 <sup>0</sup>	0.0421	0.9579	0.0405	0.9595	0.0413	0.9587
8 <sup>0</sup>	0.0424	0.9576	0.0402	0.9598	0.0413	0.9587
9 <sup>0</sup>	0.0427	0.9573	0.0399	0.9601	0.0413	0.9587
10 <sup>0</sup>	0.0430	0.9570	0.0396	0.9604	0.0413	0.9587
11 <sup>0</sup>	0.0434	0.9566	0.0393	0.9607	0.0413	0.9587
12 <sup>0</sup>	0.0438	0.9562	0.0389	0.9611	0.0413	0.9587
13 <sup>0</sup>	0.0442	0.9558	0.0385	0.9615	0.0413	0.9587
14 <sup>0</sup>	0.0447	0.9553	0.0380	0.9620	0.0413	0.9587
15 <sup>0</sup>	0.0452	0.9548	0.0375	0.9625	0.0414	0.9586
16 <sup>0</sup>	0.0458	0.9542	0.0370	0.9630	0.0414	0.9586
17 <sup>0</sup>	0.0464	0.9536	0.0364	0.9636	0.0414	0.9586
18 <sup>0</sup>	0.0471	0.952	0.0359	0.9641	0.0415	0.9585
19 <sup>0</sup>	0.0478	0.9522	0.0352	0.9648	0.0415	0.9585
20 <sup>0</sup>	0.0485	0.9515	0.0346	0.9654	0.0416	0.9584
21 <sup>0</sup>	0.0494	0.9506	0.0339	0.9661	0.0416	0.9584
22 <sup>0</sup>	0.0502	0.9498	0.0332	0.9668	0.0417	0.9583
23 <sup>0</sup>	0.0512	0.9488	0.0324	0.9676	0.0418	0.9582
24 <sup>0</sup>	0.0521	0.9479	0.0316	0.9684	0.0419	0.9581
25 <sup>0</sup>	0.0532	0.9468	0.0308	0.9692	0.0420	0.9580
26 <sup>0</sup>	0.0543	0.9457	0.0299	0.9701	0.0421	0.9579
27 <sup>0</sup>	0.0555	0.9445	0.0290	0.9710	0.0423	0.9577
28 <sup>0</sup>	0.0567	0.9433	0.0281	0.9719	0.0424	0.9576
29 <sup>0</sup>	0.0581	0.9419	0.0271	0.9729	0.0426	0.9574
30 <sup>0</sup>	0.0595	0.9405	0.0262	0.9738	0.0428	0.9572
31 <sup>0</sup>	0.0610	0.9390	0.0251	0.9749	0.0431	0.9569
32 <sup>0</sup>	0.0626	0.9374	0.0241	0.9759	0.0433	0.9567
33 <sup>0</sup>	0.0643	0.9357	0.0230	0.9770	0.0437	0.9563
34 <sup>0</sup>	0.0661	0.9339	0.0219	0.9781	0.0440	0.9560
35 <sup>0</sup>	0.0680	0.9320	0.0208	0.9792	0.0444	0.9556
36 <sup>0</sup>	0.0700	0.9300	0.0197	0.9803	0.0448	0.9552
37 <sup>0</sup>	0.0721	0.9279	0.0185	0.9815	0.0453	0.9547
38 <sup>0</sup>	0.0743	0.9257	0.0173	0.9827	0.0458	0.9542
39 <sup>0</sup>	0.0767	0.9233	0.0161	0.9839	0.0464	0.9536
40 <sup>0</sup>	0.0793	0.9207	0.0149	0.9851	0.0471	0.9529
41 <sup>0</sup>	0.0819	0.9181	0.0137	0.9863	0.0478	0.9522

$\theta_0$	$R_{\perp}$	$T_{\perp}$	$R_{\parallel}$	$T_{\parallel}$	$R_{nat}$	$T_{nat}$
42 <sup>0</sup>	0.0848	0.9152	0.0125	0.9875	0.0486	0.9514
43 <sup>0</sup>	0.0878	0.9122	0.0113	0.9887	0.0495	0.9505
44 <sup>0</sup>	0.0910	0.9090	0.0101	0.9899	0.0505	0.9495
45 <sup>0</sup>	0.0944	0.9056	0.0089	0.9911	0.0516	0.9484
46 <sup>0</sup>	0.0980	0.9020	0.0077	0.9923	0.0529	0.9471
47 <sup>0</sup>	0.1018	0.8982	0.0066	0.9934	0.0542	0.9458
48 <sup>0</sup>	0.1058	0.8942	0.0055	0.9945	0.0557	0.9443
49 <sup>0</sup>	0.1102	0.8898	0.0045	0.9955	0.0573	0.9427
50 <sup>0</sup>	0.1147	0.8853	0.0035	0.9965	0.0591	0.9409
51 <sup>0</sup>	0.1196	0.8804	0.0026	0.9974	0.0611	0.9389
52 <sup>0</sup>	0.1248	0.8752	0.0018	0.9982	0.0633	0.9367
53 <sup>0</sup>	0.1303	0.8697	0.0012	0.9988	0.0657	0.9343
54 <sup>0</sup>	0.1361	0.8639	0.0006	0.9994	0.0684	0.9316
55 <sup>0</sup>	0.1423	0.8577	0.0002	0.9998	0.0713	0.9287
56 <sup>0</sup>	0.1489	0.8511	0.0000	1.0000	0.0745	0.9255
57 <sup>0</sup>	0.1560	0.8440	0.0000	1.0000	0.0780	0.9220
58 <sup>0</sup>	0.1635	0.8365	0.0003	0.9997	0.0819	0.9181
59 <sup>0</sup>	0.1715	0.8285	0.0008	0.9992	0.0862	0.9138
60 <sup>0</sup>	0.1800	0.8200	0.0017	0.9983	0.0908	0.9092
61 <sup>0</sup>	0.1891	0.8109	0.0029	0.9971	0.0960	0.9040
62 <sup>0</sup>	0.1988	0.8012	0.0045	0.9955	0.1017	0.8983
63 <sup>0</sup>	0.2091	0.7909	0.0067	0.9933	0.1079	0.8921
64 <sup>0</sup>	0.2202	0.7798	0.0093	0.9907	0.1147	0.8853
65 <sup>0</sup>	0.2319	0.7681	0.0126	0.9874	0.1223	0.8777
66 <sup>0</sup>	0.2445	0.7555	0.0167	0.9833	0.1306	0.8694
67 <sup>0</sup>	0.2579	0.7421	0.0215	0.9785	0.1397	0.8603
68 <sup>0</sup>	0.2722	0.7278	0.0272	0.9728	0.1497	0.8503
69 <sup>0</sup>	0.2875	0.7125	0.0340	0.9660	0.1607	0.8393
70 <sup>0</sup>	0.3038	0.6962	0.0420	0.9580	0.1729	0.8271
71 <sup>0</sup>	0.3212	0.6788	0.0513	0.9487	0.1863	0.8137
72 <sup>0</sup>	0.3398	0.6602	0.0622	0.9378	0.2010	0.7990
73 <sup>0</sup>	0.3597	0.6403	0.0748	0.9252	0.2173	0.7827
74 <sup>0</sup>	0.3809	0.6191	0.0894	0.9106	0.2352	0.7648
75 <sup>0</sup>	0.4036	0.5964	0.1062	0.8938	0.2549	0.7451
76 <sup>0</sup>	0.4279	0.5721	0.1255	0.8745	0.2767	0.7233
77 <sup>0</sup>	0.4538	0.5462	0.1478	0.8522	0.3008	0.6992
78 <sup>0</sup>	0.4814	0.5186	0.1733	0.8267	0.3274	0.6726
79 <sup>0</sup>	0.5110	0.4890	0.2026	0.7974	0.3568	0.6432
80 <sup>0</sup>	0.5425	0.4575	0.2362	0.7638	0.3894	0.6106
81 <sup>0</sup>	0.5762	0.4238	0.2746	0.7254	0.4254	0.5746
82 <sup>0</sup>	0.6121	0.3879	0.3186	0.6814	0.4654	0.5346
83 <sup>0</sup>	0.6505	0.3495	0.3690	0.6310	0.5098	0.4902

$\theta_0$	$R_{\perp}$	$T_{\perp}$	$R_{\parallel}$	$T_{\parallel}$	$R_{nat}$	$T_{nat}$
$84^0$	0.6914	0.3086	0.4267	0.5733	0.5591	0.4409
$85^0$	0.7350	0.2650	0.4927	0.5073	0.6139	0.3861
$86^0$	0.7816	0.2184	0.5684	0.4316	0.6750	0.3250
$87^0$	0.8311	0.1689	0.6551	0.3449	0.7431	0.2569
$88^0$	0.8839	0.1161	0.7545	0.2455	0.8192	0.1808
$89^0$	0.9402	0.0598	0.8687	0.1313	0.9044	0.0956
$90^0$	1.0000	0	1.0000	0	1.0000	0

**11-36) Esercizio n. 4 del 9/12/2011**

Con riferimento al problema precedente graficare, in funzione dell'angolo di incidenza  $\theta_0$ , i coefficienti di riflessione  $R_{\perp}$ ,  $R_{\parallel}$  e  $R_{nat}$ , nonché i coefficienti di trasmissione  $T_{\perp}$ ,  $T_{\parallel}$  e  $T_{nat}$ .

